

BELLCOMM, INC.

955 L'ENFANT PLAZA NORTH, S.W. WASHINGTON, D.C. 20024

B70 09002

SUBJECT: Time Specific Apollo Lunar Surface Accessibility for Relaxed Free Return Missions - Computer Program Description - Case 310

DATE: September 1, 1970
FROM: S. F. Caldwell

ABSTRACT

The region of the lunar surface accessible with a specified landing time and spacecraft configuration can be defined in approximately twenty minutes of CPU time on the Univac 1108. Accessibility can be generated for relaxed free return translunar profiles with a post periselene DPS abort constraint as well as for non-free return translunar trajectories.

Program technical descriptions including flowcharts and listings are presented in sufficient detail to allow the potential user to become familiar with the underlying theory as well as the program logic.

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MEMORANDUM FOR FILE

Introduction

A new method of generating lunar surface accessibility by establishing extremals for a set of mission design parameters including the effect of a sun elevation constraint at lunar landing has been developed. Reference 1 discusses the method used and presents results for April, 1971 with the J-mission spacecraft configuration and constraints. The computer programs which were written to implement the method are described here with flowcharts and listings. Characteristic velocities are computed using patched conic analysis but corrections for the difference between integrated and patched conic trajectories are made before computing the accessibility boundary.

The accessible regions are defined by scanning all possible trajectory configurations within the mission design constraints. The feasible region defined by the limiting configurations or extremals of the trajectory geometry allowed for any specified lunar arrival time is scanned by means of three free variables: the selenocentric flight path azimuth, α , at MSI entrance, which establishes a family of lunar approach hyperbolas and is bounded by the DPS abort constraint; the angle, ϕ , between the approach hyperbola plane and the final parking orbit; and the coast angle, τ , in the parking orbit from LOI to the landing site. Defining REVLO1 to be the minimum number of orbits to be completed prior to LM landing τ is constrained to be between REVLO1 * 360 and (REVLO1 + 1) * 360. The following diagram graphically illustrates the order of scanning that is used.

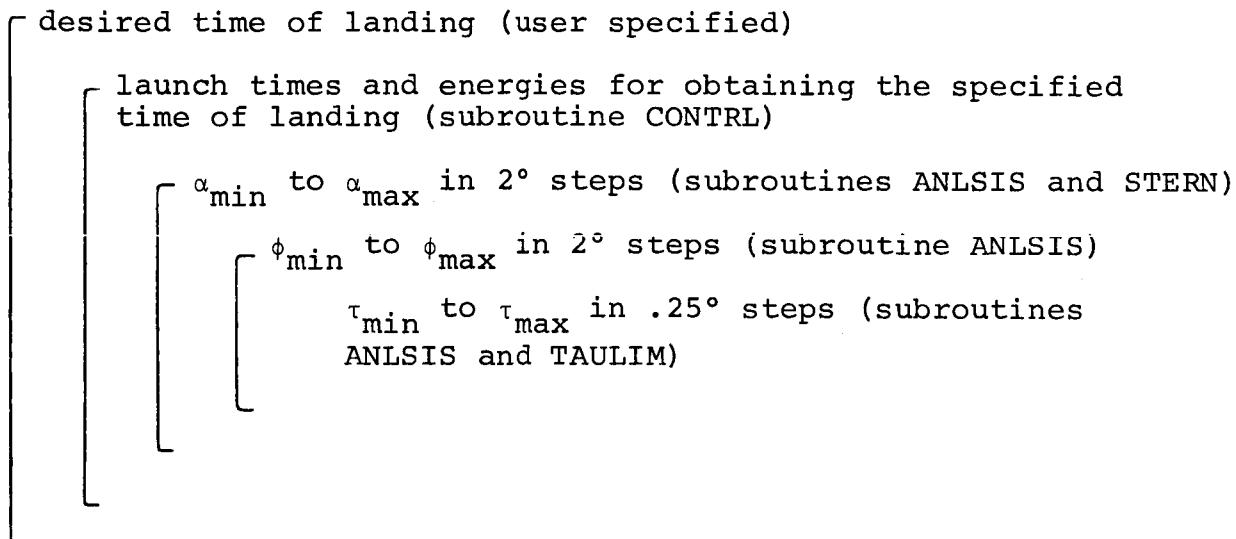


Figure 1 shows a typical lunar surface accessibility contour for one time of landing.

Launch Date and Translunar Energy Selection

CONTRL has as its inputs the desired date and time of lunar landing. From this the desired time of LOI is calculated based on a τ of (REVLOI + .5) * 360. An internal subroutine GETERG is called to obtain the translunar injection energy for a given launch day with the desired time of LOI. CTRL considers all possible launch dates that will give a translunar flight time within the mission constraints and calls subroutine ANLSIS for each to obtain the accessible area of the moon. Before returning, CTRL calls subroutine PLOT to plot the accessible area both on the printout and on the SC4020 plotter.

Appendix A contains a listing of CTRL.

α Limits

Subroutine ANLSIS finds the minimum and maximum α based on a DPS abort constraint two hours past periselene (DV9MX). For each α considered the spacecraft is targeted to the MSI by subroutine STERN* and the DPS abort ΔV (ΔV_9) is computed. α is stepped from 220° to 320° ** in 2° steps until a ΔV_9 is found less than DV9MX or ΔV_9 starts increasing (in the latter case CTRL selects another launch date and energy as this one will not meet the DPS abort constraint). Once the DV9MX boundary has been crossed, a straight line fit is used to obtain the α (α_{\min}) which has a ΔV_9 within a specified tolerance of DV9MX. α_{\max} can be obtained in the same manner by stepping α from 320° to α_{\min} in increments of -2° .

ϕ Limits

The maximum plane change (ϕ) possible at LOI must be defined for each α considered between α_{\max} and α_{\min} . Plane changes can be made either to the left or the right relative to the incoming hyperbola. A sign convention has been assumed to

*See Appendix B for a discussion and listing of STERN.

**For retrograde lunar orbits α is limited to 180° to 360° . Imposing a DPS abort constraint eight hours past periselene reduces the α range. In all cases an α range of 220° to 320° was found to be sufficient.

distinguish these two directions: a plane change to the left is negative and a plane change to the right is positive. Thus the largest ϕ made to the left can be called ϕ_{\min} and the largest to the right, ϕ_{\max} .

Propellant requirements are defined by the three mission dependent maneuvers; LOI, plane change prior to rendezvous (PCM), and TEI. The magnitude of ϕ defines the LOI ΔV as there is no flight path angle change at LOI.* Selection of the point under the resulting orbit subsequently defines PCM ΔV and TEI ΔV . One point under each orbit requires no PCM. ϕ_{\min} allows landing at that point, with LOI and TEI consuming all the available SPS propellant. ϕ_{\max} is the largest right oriented plane change that can be accomplished, similarly landing under the orbit where a CSM plane change prior to rendezvous is unnecessary and LOI and TEI consume all the available propellant. ϕ 's between ϕ_{\min} and ϕ_{\max} generate LOI and TEI ΔV 's that do not consume all the propellant; the remaining propellant can be used for the PCM. The ϕ extremals are computed by subroutine ANLSIS.

τ Limits

For each ϕ between ϕ_{\min} and ϕ_{\max} the τ limits are computed by subroutine TAULIM.** Using one of the limits returned by TAULIM the trajectory is targeted to earth landing*** and the total propellant burned (FUEL) based on the current ΔV budget is computed by subroutine WGBTUD.**** By comparing FUEL to the total propellant available (FUELMX) a CSM plane change ΔV is computed to use all the remaining available propellant. τ limits based on

*A parametric study has shown that off perilune deboost into lunar orbit does not appreciably increase the accessible region. In some cases, however, off perilune LOI does reduce ΔV costs to a site within the accessible region.

**Appendix C contains a discussion, listing and flowchart of TAULIM.

***Subroutine GNDHOM is used to generate a fuel optimal transearth trajectory from lunar parking orbit to earth landing. The trajectory is fuel optimized within the constraints with respect to longitude of earth landing and time of flight. FLYHOM is a subroutine used by GNDHOM. Reference 2 contains a discussion of GNDHOM and FLYHOM.

****Reference 3 contains a discussion of the method used in WGBTUD.

this CSM plane change ΔV are then obtained. This iterative procedure is repeated (for both τ_{\min} and τ_{\max}) until a trajectory is obtained that uses all the available propellant. For each τ between τ_{\min} and τ_{\max} the point on the lunar surface where landing is possible is calculated and compared against the periphery matrix by subroutine SAVE.

Accessibility Periphery

Subroutine SAVE collects the periphery matrix of accessibility between longitudes of $\pm 60^\circ$. The periphery is collected for every half degree of longitude. For each longitude the minimum and maximum latitude is saved. The periphery matrix is initialized once for each desired lunar landing time. Upon entering SAVE the latitude of the lunar landing site is compared to the minimum and maximum latitude in the periphery matrix corresponding to the longitude of the lunar landing site. If an improvement is made the periphery matrix is updated. In conjunction with the periphery matrix there is a data matrix so that each point in the periphery matrix can be identified. The data matrix stores the date and time of launch; the date and time of MSI entrance; the date and time of lunar landing; α ; whether the α was a minimum or maximum; the translunar injection energy; whether or not the point was generated by ϕ_{\min} , ϕ_{\max} , τ_{\min} or τ_{\max} ; and whether the whole orbit was accessible.

Subroutine ANLSIS contains four internal subroutines: GNDHOM, FLYHOM, SAVE and WGBTUD. Appendix D contains a flowchart of ANLSIS and a listing of ANLSIS and its internal subroutines.

Plots (Subroutine PLOT)

The input to PLOT is the periphery matrix that was collected for one lunar arrival time. The entire periphery matrix is plotted on the on line printer and a smoothed periphery matrix is plotted on the SC4020 plotter. Figure 1 shows a sample SC4020 plot. The plotting package used was AUPLLOT, a description of which can be found in Reference 4.

Appendix E contains a listing of PLOT.

Remarks

On the Univac 1108 the generation of the lunar surface accessible for one landing time takes approximately 20 minutes of CPU time or about 170 charge units. At the present time the program will compute relaxed free return translunar trajectories

with a DPS abort constraint. The DPS abort constraint could be removed by performing minor modifications to the program ANLSIS. Monitoring of the RCS abort capability is not currently included.

For each arrival time the entire periphery matrix and data matrix are punched on cards. These cards can be used to determine the accessible areas for various lighting constraints or the accessible area by launch date. Reference 5 contains the accessible region of the lunar surface for a lighting constraint of 5° to 14° and 20° to 30° and the accessible regions by launch date for both November and December, 1971.

S F Caldwell

2013-SFC-slr

S. F. Caldwell

Attachments

BELLCOMM, INC.

REFERENCES

1. Bass, R. A. and Stern, R. J., "Determination of Apollo Lunar Surface Accessibility Subject to DPS Abort and Lighting Constraints," Bellcomm Technical Memorandum TM-70-2013-2, March 31, 1970.
2. Kerr, M. R. and Stern, R. J., "An Improved Determination of Optimal Moon-to-Earth Trajectories for BCMASP," Bellcomm Memorandum for File B70 04050, April 20, 1970.
3. McGarry, C. L., "Spacecraft Weight and ΔV Budget Program on the IBM Terminal," Working Note to D. R. Anselmo, February 18, 1970.
4. Jessup, R. F., "The AUPLLOT Graphical Data Processing System," Bellcomm Memorandum for File B69 10117, October 27, 1969.
5. Bass, R. A., "J-Mission Lunar Accessibility During November and December, 1971," Bellcomm Memorandum for File B70 07017, July 7, 1970.

APPENDIX A

CTRL

Calling Sequence: CALL CTRL (DATEAR, TIMEAR)

Purpose: CTRL determines all possible launch times and translunar injection energies for a specified time of lunar landing.

Input:

DATEAR - Desired date of lunar landing
TIMEAR - Desired time of lunar landing

```

C          000100A1
C          SUBROUTINE CONTRL(DATEAR,TIMEAR)          000200A1
C          000300A1
C          COMMON/OLDNEW/IPLOT          000400A1
C          COMMON/C4/TWV(400)/C5/FLT(130)/C7/PHC(50) 000500A1
C          EQUIVALENCE          (FLT( 7),DATEF ), (FLT( 8),TIMEF ), 000500A1
C          1(FLT( 24),RM9R ), (FLT( 32),RL0 ), (FLT( 33),REVL01), 000700A1
C          2(PHC( 15),RM ), (PHC( 25),GMM ), (PHC( 33),PI ), 000800A1
C          3(PHC( 37),HRDAY ), (PHC( 40),FTMILE ), (PHC( 43),SECHR ), 000900A1
C          4(TWV( 35),DATELP ), (TWV( 35),TIMELP ), (TWV( 38),TPFLT ), 001000A1
C          5(TWV( 40),TEOP ), (TWV( 45),ERG7P ), (TWV( 46),DAT8P ), 001100A1
C          6(TWV( 47),TIM8P ), (TWV( 57),RM8PX ), (TWV( 51),VM8PX ), 001200A1
C          7(TWV( 71),RM9RP ), (TWV(259),DAT20P ), (TWV(260),TIM20P ), 001300A1
C          8(TWV(262),SVHRTL), (TWV(381),ALPHA )          001400A1
C          DIMENSION RM20PX(3), VM20PX(3), RM8PX(3), D(3), E(3), T(3) 001500A1
C          001600A1
C          ALPHA=270.          001700A1
C          RM9RPERM9R          001800A1
C          PERLOP=2.*PI*RL0*SQRT(RL0/GMM)          001900A1
C          CALL ADDT(DATEAR,TIMEAR,0.,-(REV-01+.5)*PERLOP,DAT20R,TIM20R) 002000A1
C          DATEF=DAT20R-4.          002100A1
C          TIMEF=TIM20R          002200A1
C          CALL GETERG          002300A1
C          I=1          002400A1
C          D(I)=DATEF          002500A1
C          T(I)=TIMEF          002600A1
C          E(I)=ERG7P          002700A1
C          002800A1
C          IF(HRTP-24..LT.60.)GO TO 10          002900A1
C          I=I+1          003000A1
C          D(I)=DATEF+1.          003100A1
C          003200A1
C          IF(HRTP-48..LT.60.)GO TO 10          003300A1
C          I=I+1          003400A1
C          D(I)=DATEF+2.          003500A1
C          003600A1
C          10 IF(HRTP+24.GT.110)GO TO 20          003700A1
C          I=I+1          003800A1
C          D(I)=DATEF-1.          003900A1
C          004000A1
C          IF(HRTP+48.GT.110)GO TO 20          004100A1
C          I=I+1          004200A1
C          D(I)=DATEF-2.          004300A1
C          GO TO 20          004400A1
C          004500A1
C          20 DO 30 J=2,I          004600A1
C          DATEF=D(J)          004700A1
C          CALL GETERG          004800A1
C          IF(<20.EQ.20.AND.ABS(HRTP-HRTLR).GE..1)GO TO 40          004900A1
C          30 E(J)=ERG7P          005000A1
C          T(J)=TIMEF          005100A1
C          GO TO 50          005200A1
C          40 I=I-1          005300A1
C          50 CALL INIT          005400A1

```

```

IPLOT=0          005500A1
DO 60 I2=1,I    005600A1
DATEF=D(I2)      005700A1
TIMEF=T(I2)      005800A1
ERG7P=E(I2)      005900A1
50 CALL ANLSIS   006000A1
IF(IPLOT.NE.0)CALL PLOT 006100A1
RETURN          006200A1
C
C
C
SUBROUTINE GETERG 006300A1
K20=1            006400A1
ERG7P=-8000000.  006500A1
DERG7P=-500000.  006600A1
10 CALL STERN    006700A1
CALL CONIC(RMBPX,VMBPX,1,1,RL0,RM20PX,VM20PX,TEMP50) 006800A1
CALL ADDT(DAT8P,TIM8P,0.,TEMP50,DAT20P,TIM20P)        006900A1
HRTLP=(DAT20P-DATEF)*HRDAY+(TIM20P-TIMEF-TPFLT-TEOP)/SECHR 007000A1
HRTLRL=(DAT20R-DATEF)*HRDAY+(TIM20R-TIMEF-TPFLT-TEOP)/SECHR 007100A1
CALL PRINTR(0,'DATEF TIMEF ERG7P HRTLP RTLRL ', 007200A1
.DATEF,TIMEF,ERG7P,HRTLP,HRTLRL)                      007300A1
C
IF(ABS(HRTLP-HRTLRL).LT..1.0R.K20.EQ.20)RETURN 007400A1
IF(K20.EQ.1)GO TO 25 007500A1
SHRTL=(HRTLP-HRTLRL)/DERG7P 007600A1
DERG7P=(HRTLRL-HRTLP)/SHRTL 007700A1
IF(ABS(DERG7P).LT..1.E6)GO TO 25 007800A1
DERG7P=SIGN(1.E6,DERG7P) 007900A1
20 SHRTL=HRTLP 008000A1
ERG7P=ERG7P+DERG7P 008100A1
K20=K20+1 008200A1
GO TO 10 008300A1
C
END          008400A1
008500A1
008600A1
008700A1
008800A1
008900A1

```

APPENDIX B

STERN

Calling Sequence: CALL STERN

Purpose: STERN is used by subroutine ANLSIS to target the spacecraft from launch to the moon's sphere of influence (MSI). The trajectory is constrained to yield a periselene radius of 60 n.mi.*

Input:

PHIMSP - Latitude of previous MSI entrance point
XLMMSP - Longitude of previous MSI entrance point
ALPHA - Selenocentric flight path azimuth at MSI entrance

Output:

PHIMSP - Latitude of MSI entrance point
XLMMSP - Longitude of MSI entrance point
RM8PX(3) - Position at MSI entrance
VM8PX(3) - Velocity at MSI entrance

Method:

STERN calls subroutine HITMSI to target the spacecraft from launch to a point on the moon's sphere of influence. Using the previous latitude (η) and longitude (ζ) of MSI entrance HITMSI is called to obtain the velocity vector (\bar{v}_{MSI}) at the MSI. STERN then computes the latitude (η_0) and longitude (ζ_0) of the negative \bar{v}_{MSI} pierce point. Since the translunar injection energy is defined and the periselene radius is fixed the desired MSI pierce point lies on the dotted circle in Figure 2.

The flight path angle, β , can be computed using basic equations for orbital mechanics. The following definitions were used for the semilatus rectum (p), the orbit eccentricity (e), the semimajor axis (a), and the angular momentum (h).

*A parametric study has shown that perilune depression to 40 n.mi. does not increase the accessible region.

$$p = \frac{h^2}{\mu} = r_p (1+e) \quad (B1)$$

$$e = 1 - \frac{r_p}{a}$$

$$a = \left(\frac{2}{r} - \frac{v^2}{\mu} \right)^{-1}$$

$$h = rV \sin\beta$$

r is the radius of the moon, V is the velocity magnitude at MSI entrance, and r_p is the desired periselene radius. Substituting in Equation (B1) for h , e and a gives

$$\frac{r^2 v^2 \sin^2 \beta}{\mu} = 2r_p - r_p^2 \left(\frac{2}{r} - \frac{v^2}{\mu} \right).$$

Dividing both sides of the equation by $\frac{r^2 v^2}{\mu}$,

$$\sin^2 \beta = \frac{2r_p \mu}{r^2 v^2} - r_p^2 \left(\frac{2\mu}{r^3 v^2} - \frac{1}{r^2} \right)$$

collecting terms and taking the square root gives an equation for $\sin\beta$.

$$\sin\beta = \frac{r_p}{r} \left[1 + \frac{2\mu}{r_p v^2} \left(1 - \frac{r_p}{r} \right) \right]^{1/2}$$

The desired pierce point (η , ζ) for a given α can then be calculated using the law of sines and cosines.

$$\cos\left(\frac{\pi}{2}-\eta\right) = \cos\left(\frac{\pi}{2}-\eta_0\right) \cos\beta + \sin\left(\frac{\pi}{2}-\eta_0\right) \sin\beta \cos\alpha$$

or

$$\eta = \sin^{-1} (\sin\eta_0 \cos\beta + \cos\eta_0 \sin\beta \cos\alpha)$$

and

$$\frac{\sin\alpha}{\sin\left(\frac{\pi}{2}-\eta\right)} = \frac{\sin(\zeta-\zeta_0)}{\sin\beta}$$

or

$$\zeta = \zeta_0 + \sin^{-1} \left(\frac{\sin\alpha \sin\beta}{\cos\eta} \right)$$

If this η and ζ are not within some specified tolerance of the ones that were imputed to HITMSI the whole process is repeated.

```

C                               000100A1
C                               000200A1
C                               000300A1
C                               000400A1
C                               000500A1
C                               000600A1
C                               000700A1
C                               000800A1
C                               000900A1
C                               001000A1
C                               001100A1
C                               001200A1
C                               001300A1
C                               001400A1
C                               001500A1
C                               001600A1
C                               001700A1
C                               001800A1
C                               001900A1
C                               002000A1
C                               002100A1
100    C1=C1+1
C                               002200A1
C                               002300A1
C                               002400A1
C                               002500A1
C                               002600A1
C                               002700A1
C                               002800A1
C                               002900A1
C                               003000A1
C                               003100A1
C                               003200A1
C                               003300A1
C                               003400A1
C                               003500A1
C                               003600A1
C                               003700A1
C                               003800A1
C                               003900A1
C                               004000A1
C                               004100A1
C                               004200A1
C                               004300A1
C                               004400A1
200    IF(ABS(DELT8).GT.1.)WRITE(6,201)DELT8
201    FORMAT(' ***HITMSI DID NOT CONVERGE',2E16.8)
      RETURN
C                               004500A1
C                               004600A1
C                               004700A1
C                               004800A1
150    WRITE(6,1)PHIMSP,PHINEW,XLMMSP,XLMNEW
1      FORMAT(' ***C1=20 IN STERN PHIMSP',2E14.8,5X,'XLMMSP',2E14.8)
      GO TO 200
      END
      004900A1
      005000A1
      005100A1
      005200A1

```

APPENDIX C

TAULIM

Calling Sequence: CALL TAULIM (RM21PX, VM21PX, HMLOPX, DLV55P,
TAUL, IORBIT)

Purpose: For a given CSM plane change TAULIM computes the minimum
and maximum coast angle, τ , in the parking orbit from LOI to the
landing site.

Input:

RM21PX(3)	- Position vector after LOI
VM21PX(3)	- Velocity vector after LOI
HMLOPX(3)	- Angular momentum vector
DLV55P	- CSM plane change
REVL01	- Minimum number of orbits to be completed prior to landing
HRSTAY	- Lunar surface stay time
RTOD	- Conversion factor - radians to degrees
PERLOP	- Period of lunar orbit

Output:

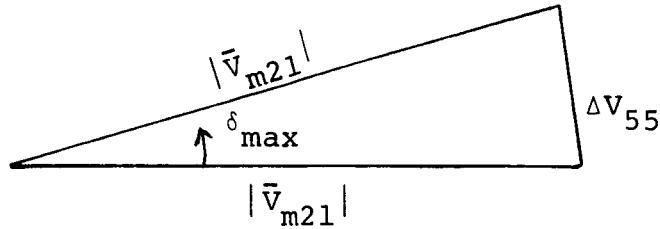
TAUL(2)	- Minimum (TAUL ₍₁₎) and maximum (TAUL ₍₂₎) τ
IORBIT	- Flag denoting whether whole orbit is accessible, 1 yes, 0 no

Method:*

In Figure 3 \bar{R}_{m21} and \bar{V}_{m21} are the position and velocity
after LOI, \bar{Z} is the selenographic pole in selenographic coordi-
nates, \bar{R} is the position of the CSM above the landing site after
LM descent, \bar{R}' is the position of the CSM after the lunar stay
time, \bar{H}_{mlop} is $\bar{R}_{m21} \times \bar{V}_{m21}$ and θ_m is the lunar stay time multi-
plied by the rotation rate of the moon.

*Equations were obtained from hand notes of R. J. Stern.

Given a CSM plane change $\Delta V(\Delta V_{55})$ TAULIM can compute the maximum out of plane angle (δ_{\max}) after the lunar stay time.



$$\delta_{\max} = 2 \sin^{-1} \left[\frac{\Delta V_{55}}{2 |\bar{v}_{m21}|} \right]$$

From Figure 3 an equation for \bar{R} in terms of τ can be derived.

$$\frac{\bar{R}}{|\bar{R}|} = \frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \cos \tau + \frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \sin \tau \quad (C1)$$

\bar{R} can also be written as the sum of two vectors \bar{A} and \bar{B} where \bar{A} is parallel to \bar{z} and \bar{B} is perpendicular to \bar{z} .

$$\bar{A} = (\bar{R} \cdot \bar{z}) \bar{z} \quad \text{and}$$

$$\bar{B} = \bar{R} - \bar{A} \quad \text{or} \quad \bar{R} = \bar{B} + \bar{A}$$

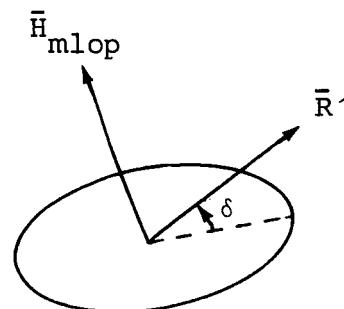
Then using Figure 3

$$\bar{R}' = \bar{B} \cos \theta_m + (\bar{z} \times \bar{B}) \sin \theta_m + \bar{A}$$

or substituting for \bar{A} and \bar{B}

$$\bar{R}' = \bar{R} \cos \theta_m + (\bar{R} \cdot \bar{Z}) (1 - \cos \theta_m) \bar{Z} + (\bar{Z} \times \bar{R}) \sin \theta_m \quad (C2)$$

From the following sketch



it can be seen that

$$\sin \delta_{\max} = \bar{H}_{mlop} \cdot \frac{\bar{R}'}{|\bar{R}'|} \quad (C3)$$

Substituting equation (C1) and (C2) into equation (C3) gives

$$\begin{aligned}
 \bar{H}_{mlop} \cdot & \left[\frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \cos\tau \cos\theta_m + \frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \sin\tau \cos\theta_m \right] \\
 & + \bar{H}_{mlop} \cdot \left[(1-\cos\theta_m) \left\{ \cos\tau \left(\frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \cdot \bar{z} \right) + \sin\tau \left(\frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \cdot \bar{z} \right) \right\} \bar{z} \right] \\
 & + \bar{H}_{mlop} \times \left[\bar{z} \times \left(\frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \cos\tau + \frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \sin\tau \right) \right] \sin\theta_m - \sin\delta_{max} = 0
 \end{aligned}$$

Using the scalar triple product and defining α , β , and γ

$$\begin{aligned}
 \alpha &= (1-\cos\theta_m) (\bar{H}_{mlop} \cdot \bar{z}) \left(\bar{z} \cdot \frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \right) \\
 &+ \sin\theta_m \left(\frac{\bar{R}_{m21}}{|\bar{R}_{m21}|} \cdot (\bar{H}_{mlop} \times \bar{z}) \right)
 \end{aligned}$$

$$\begin{aligned}
 \beta &= (1-\cos\theta_m) (\bar{H}_{mlop} \cdot \bar{z}) \left(\bar{z} \cdot \frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \right) \\
 &+ \sin\theta_m \left(\frac{\bar{v}_{m21}}{|\bar{v}_{m21}|} \cdot (\bar{H}_{mlop} \times \bar{z}) \right)
 \end{aligned}$$

$$\gamma = \sin\delta_{max}$$

gives an expression in terms of τ

$$\alpha \cos\tau + \beta \sin\tau - \gamma = 0 \quad (C4)$$

Using the identity

$$\sin\tau = \pm(1-\cos^2\tau)^{1/2} \quad (C5)$$

in Equation (C4) and squaring gives an equation for $\cos\tau$ by use of the quadratic equation.

$$\cos\tau = \frac{\alpha\gamma \pm \beta(\alpha^2 + \beta^2 - \gamma^2)^{1/2}}{\alpha^2 + \beta^2} \quad (C6)$$

There are three cases to be considered:

1. There is no CSM plane change prior to rendezvous. In this case ΔV_{55} , δ and hence γ would be zero and Equation (C4) reduces to

$$\tan\tau = -\frac{\alpha}{\beta}$$

2. There is a CSM plane change prior to rendezvous and $\alpha^2 + \beta^2 - \gamma^2 < 0$ (the whole orbit is accessible). When the whole orbit is accessible the largest ΔV_{55} would occur for $\gamma^2 = \alpha^2 + \beta^2$. Substituting this into Equation (C6) gives

$$\cos\tau = \frac{\alpha}{(\alpha^2 + \beta^2)^{1/2}}$$

Substituting in Equation (C4) for $\cos\tau$ an equation is derived for $\sin\tau$.

$$\sin\tau = \frac{\beta}{(\alpha^2 + \beta^2)^{1/2}}$$

Therefore,

$$\tan\tau = \frac{\beta}{\alpha}$$

3. There is a CSM plane change prior to rendezvous and $\alpha^2 + \beta^2 - \gamma^2 > 0$. Using Equations (C6) and (C5) there are four possible τ 's, two of which are extraneous due to Equation (C5). The two τ 's that satisfy Equation (C4) are the desired τ 's (τ_{al} and τ_{a2} with $\tau_{al} < \tau_{a2}$).

For all three cases the τ 's for $+\delta_{max}$ have been found. From Equation (C4) it can be seen that the τ 's corresponding to $-\delta_{max}$ are 180° away from the τ 's corresponding to $+\delta_{max}$. For case #1 where there is no CSM plane change there are only two possible τ 's. For this case the τ corresponding to $+\delta_{max}$ is returned. For case #2 where the whole orbit is accessible τ_{min} and τ_{max} are set to the worst possible cases. For case #3 where only portions of the orbit are accessible the τ limits are more difficult to determine. The τ 's corresponding to $-\delta_{max}$ are

$$\tau_{b2} = \tau_{al} + 180^\circ$$

$$\tau_{bl} = \tau_{a2} + 180^\circ$$

The possible τ regions are shown by the shaded areas in Figure 4. The CSM plane change and TEI ΔV 's are the same for τ 's between τ_{a1} and τ_{b1} as for τ 's between τ_{a2} and τ_{b2} , so only one of these regions needs to be considered. TAULIM returns that region which is entirely within the one orbit. If both regions are within the one orbit the earliest one is returned. The τ region returned is the shaded area that is not cross hatched in Figure 4.

```

C          SUBROUTINE TAULIM(RM21PX,VM21PX,HMLOPX,DLV55P,TAUL,IORBIT)      000100A1
C
C          COMMON/VALUES/SLOV(241),SLAT(241,2),ITVAL(6,241)           000200A1
C          COMMON/C4/TWV(400)/C5/FLT(130)/C7/PHC(50)           000300A1
C          EQUIVALENCE           (FLT(33),REVL01),   (FLT(35),HRSTAY), 000400A1
C          1(PHC(35),RT00),    (TWV(131),PERLOP)           000500A1
C          DIMENSION HMLOPX(3), RM21PX(3), VM21PX(3), TAJA(2), TAJB(2), 000600A1
C          1A(3), Z(3), TEMP1(3), TAUL(2), COSTAJ(2), SINTAJ(2), T(4) 000700A1
C          OMEGA=.00015250437                                     000800A1
C          TAUR1=REVL01*360.                                     000900A1
C          TSTAY=AINT(HRSTAY*3600./PERLOP+.25)*PERLOP        001000A1
C          THETAM=OMEGA*TSTAY/RT00                            001100A1
C          A(1)=0.                                              001200A1
C          A(2)=0.                                              001300A1
C          A(3)=1.                                              001400A1
C          CALL M=IXP(0,A,Z)                                    001500A1
C
C          DELMAX=2.*ARSIN(DLV55P/(2.*VALJE(VM21PX)))       001600A1
C          TEMP50=(1.-COS(THETAM))*DOT(HMLOPX,Z)           001700A1
C          CALL CROSS(HMLOPX,Z,TEMP1,0)                      001800A1
C          ALFA=TEMP50*DOT(Z,RM21PX)/VALJE(RM21PX)+SIN(THETAM)*DOT(RM21PX, 001900A1
C          1TEMP1)/VALJE(RM21PX)                           002000A1
C          BETA=TEMP50*DOT(Z,VM21PX)/VALJE(VM21PX)+SIN(THETAM)*DOT(VM21PX, 002100A1
C          1TEMP1)/VALJE(VM21PX)                           002200A1
C          GAMMA=SIN(DELMAX)                                002300A1
C
C          IORBITE=0                                         002400A1
C          IF(DLV55P.GT.0)GO TO 100                         002500A1
C          TAJL(1)=RT00*ATAN2(-ALFA/BETA,1.)               002600A1
C          IF(TAJL(1).LT.0.)TAJL(1)=TAUL(1)+360.          002700A1
C          TAJL(1)=TAJL(1)+TAUR1                          002800A1
C          RETURN                                            002900A1
C
C 100   TEMP50=ALFA**2+BETA**2                         003000A1
C          TEMP51=TEMP50-GAMMA**2                         003100A1
C          IF(TEMP51.GT.0.)GO TO 200                     003200A1
C          IORBITE=1                                       003300A1
C          TAUL(1)=RT00*ATAN2(BETA,ALFA)                 003400A1
C          IF(TAJL(1).LT.0.)TAJL(1)=TAUL(1)+180.         003500A1
C          TAJL(1)=TAJL(1)+TAUR1                          003600A1
C          TAJL(2)=TAJL(1)+180.                           003700A1
C          RETURN                                            003800A1
C
C 200   TEMP52=ALFA*GAMMA/TEMP50                         003900A1
C          TEMP53=BETA*SQRT(TEMP51)/TEMP50              004000A1
C          COSTAJ(1)=TEMP52+TEMP53                      004100A1
C          COSTAJ(2)=TEMP52-TEMP53                      004200A1
C          SINTAJ(1)=SQRT(1.-COSTAJ(1)**2)            004300A1
C          SINTAJ(2)=SQRT(1.-COSTAJ(2)**2)            004400A1
C          T(1)=ABS(ALFA*COSTAJ(1)+BETA*SINTAJ(1)-GAMMA) 004500A1
C          T(2)=ABS(ALFA*COSTAJ(1)-BETA*SINTAJ(1)-GAMMA) 004600A1
C          T(3)=ABS(ALFA*COSTAJ(2)+BETA*SINTAJ(2)-GAMMA) 004700A1
C

```

```

T(4)=ABS(ALFA*COSTAJ(2)-BETA*SINTAJ(2)-GAMMA)          005500A1
J=1              005600A1
DO 210 I=2,4      005700A1
210 IF(T(I).LT.T(J))J=I      005800A1
K=1              005900A1
IF(J.EQ.1)<=2      006000A1
DO 220 I=2,4      006100A1
220 IF(T(I).LT.T(K).AND.I.NE.J)<=I      006200A1
IAVS=1          006300A1
GO TO (240,250,260,270),J      006400A1
240 TAJA(IAVS)=RTOD*ATAN2(+SINTAJ(1)*COSTAJ(1))      006500A1
GO TO 280          006500A1
250 TAJA(IAVS)=RTOD*ATAN2(-SINTAJ(1)*COSTAJ(1))      006700A1
GO TO 280          006800A1
260 TAJA(IAVS)=RTOD*ATAN2(+SINTAJ(2)*COSTAJ(2))      006900A1
GO TO 280          007000A1
270 TAJA(IAVS)=RTOD*ATAN2(-SINTAJ(2)*COSTAJ(2))      007100A1
280 IF(IAVS.EQ.2)GO TO 290      007200A1
IAVS=2          007300A1
GO TO (240,250,260,270),K      007400A1
290 IF(TAJA(1).LT.0.)TAJA(1)=TAJA(1)+360.      007500A1
IF(TAJA(2).LT.0.)TAJA(2)=TAJA(2)+360.      007600A1
IF(TAJA(1).LT.TAJA(2))GO TO 300      007700A1
TEMP50=TAJA(1)      007800A1
TAJA(1)=TAJA(2)      007900A1
TAJA(2)=TEMP50      008000A1
300 TAJB(1)=AMOD(TAJA(2)+180.,360.)+TAJR1      008100A1
TAJB(2)=AMOD(TAJA(1)+180.,360.)+TAJR1      008200A1
TAJA(1)=TAJA(1)+TAJR1      008300A1
TAJA(2)=TAJA(2)+TAJR1      008400A1
C          008500A1
IF(TAJA(2)-TAJA(1).LT.180.)GO TO 400      008500A1
TAJL(1)=TAJA(1)      008700A1
TAJL(2)=TAJB(1)      008800A1
RETURN      008900A1
C          009000A1
400 IF(ABS(TAJA(1)-TAJB(1)).GT.180.)GO TO 500      009100A1
TAJL(1)=TAJB(1)      009200A1
TAJL(2)=TAJA(1)      009300A1
RETURN      009400A1
C          009500A1
500 TAJL(1)=TAJA(2)      009600A1
TAJL(2)=TAJB(2)      009700A1
RETURN      009800A1
C          009900A1
END      010000A1

```

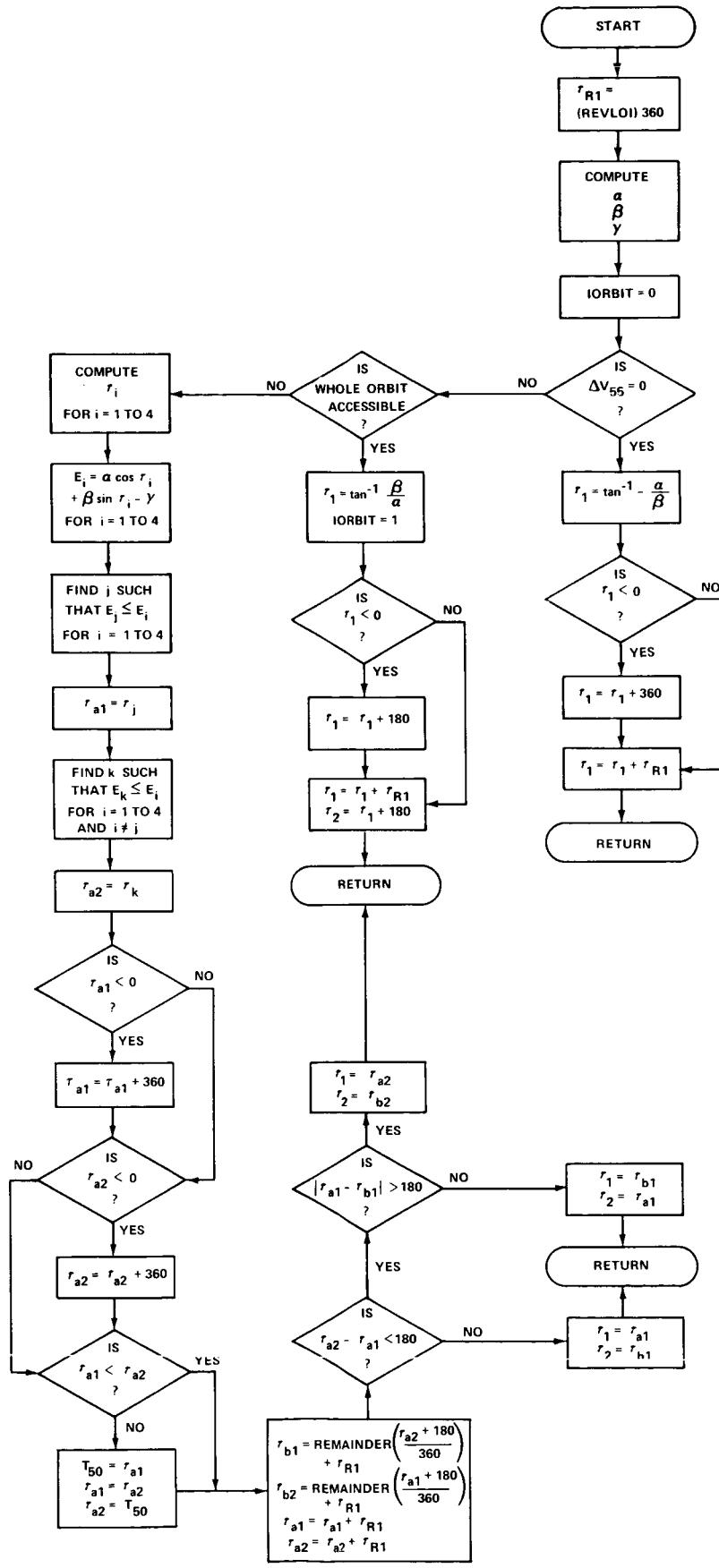


FIGURE C-1: TAULIM FLOWCHART

APPENDIX D

ANLSIS

Calling Sequence: CALL ANLSIS

Purpose: Given a date and time of launch and the translunar injection energy ANLSIS finds the boundary of the accessible region of the moon.

Input:

DATEF - Earliest possible date of launch
TIMEF - Earliest possible time of launch
ERG7P - Translunar injection energy

Output:

SLON(241) - Longitude in $.5^\circ$ from -60° to 60°
SLAT(241,2) - SLAT(I,1) is the minimum latitude and SLAT(I,2) is the maximum latitude corresponding to a longitude of SLON(I)
ITVAL(6,241) - Data matrix associated with the boundary matrix
ITVAL(J,I) - contains date and time of launch and a flag of
 0 if $\alpha \neq \alpha_{\min}$ and $\alpha \neq \alpha_{\max}$
 1 if $\alpha = \alpha_{\min}$
 2 if $\alpha = \alpha_{\max}$
ITVAL(J+1,I) - contains date and time of MSI entrance and the value of α
ITVAL(J+2,I) - contains date and time of landing, the translunar injection energy and a flag of
 1 if $\phi = \phi_{\min}$
 2 if $\phi = \phi_{\max}$
 3 if $\tau = \tau_{\min}$
 4 if $\tau = \tau_{\max}$
 5 if $\tau \neq \tau_{\min}$ and $\tau \neq \tau_{\max}$

$\left. \begin{array}{l} 3 \\ 4 \\ 5 \end{array} \right\}$ whole orbit
is not
accessible

6 if $\tau = \tau_{\min}$
7 if $\tau = \tau_{\max}$
8 if $\tau \neq \tau_{\min}$ and $\tau \neq \tau_{\max}$

} whole orbit
is accessible

J = 1 defines the data matrix for the minimum latitude,
J = 4 defines the data matrix for the maximum latitude
and I denotes the corresponding position on the longitude matrix.

C	ANLSIS	000100S1
C	SUBROUTINE ANLSIS	000200S1
C	COMMON/OLDNEW/IPLOT	000300S1
	COMMON/VALJES/SLOV(241),SLAT(241*2),ITVAL(6,241)	000400S1
	COMMON/C20/DLLMDA,DF30P,P026DT	000500S1
	COMMON/C1/VAR(375)/C4/TWV(400)/C5/FLT(130)/C6/VEH(100)/C7/PHC(50)	000600S1
	EQUIVALENCE (FLT(7),DATEF), (FLT(8),TIMEF),	000700S1
1	(FLT(15),ELTMIN), (FLT(16),ELTMAX), (FLT(18),ELNMIN),	000800S1
2	(FLT(19),ELNMAX), (FLT(22),REVEO), (FLT(26),BTA11R),	000900S1
3	(FLT(32),RL0), (FLT(33),REVLO1), (FLT(34),REVLO2),	001000S1
4	(FLT(35),HRSTAY), (FLT(36),HRTMAX), (FLT(37),BTA29R),	001100S1
5	(FLT(38),RIMAX), (FLT(39),RIMAX), (FLT(40),THMMIN),	001200S1
6	(FLT(41),THMMAX), (FLT(128),DLVTL), (FLT(129),DLVTE),	001300S1
7	(FLT(130),DLVRSC)	001400S1
	EQUIVALENCE (VEH(16),THR20), (VEH(17),WGT7),	001500S1
1	(VEH(18),DWGT20), (VEH(22),WGT40), (VEH(55),WGTAST)	001600S1
	EQUIVALENCE (PHC(1),GSTD), (PHC(2),REGEOD),	001700S1
1	(PHC(5),FLAT), (PHC(8),OMEGA), (PHC(14),ALTATM),	001800S1
2	(PHC(15),RM), (PHC(25),GMM), (PHC(28),RMSI),	001900S1
3	(PHC(33),PI), (PHC(34),DTDR), (PHC(35),RTOD),	002000S1
4	(PHC(36),DEGCIR), (PHC(40),FTMILE), (PHC(43),SECHR),	002100S1
	EQUIVALENCE (TWV(45),ERG7P), (TWV(46),DATBP),	002200S1
1	(TWV(47),TIMBP), (TWV(49),QDELT8), (TWV(60),RMSIP),	002300S1
2	(TWV(51),VM8PX), (TWV(71),RM9RP), (TWV(100),BTA11P),	002400S1
3	(TWV(101),RE11P), (TWV(122),DLV20P), (TWV(128),HML0PX),	002500S1
4	(TWV(131),PERL0P), (TWV(132),RL0P), (TWV(152),DAT25P),	002600S1
5	(TWV(153),TIM25P), (TWV(154),RM25PX), (TWV(158),DAT26P),	002700S1
6	(TWV(159),TIM26P), (TWV(162),DLV26P), (TWV(173),DAT28P),	002800S1
7	(TWV(174),TIM28P), (TWV(185),RE28PX), (TWV(188),RE28P),	002900S1
8	(TWV(194),ALF28P), (TWV(196),QALF28), (TWV(207),BTA29P),	003000S1
9	(TWV(209),DAT30P), (TWV(210),TIM30P), (TWV(212),QDLT30),	003100S1
.	(TWV(213),HRTEP), (TWV(214),THETAM), (TWV(215),RENTC1),	003200S1
1	(TWV(216),RENTC2), (TWV(217),ELT30R), (TWV(218),ELN30R),	003300S1
2	(TWV(219),ELT30P), (TWV(220),ELN30P), (TWV(221),QEL30),	003400S1
3	(TWV(226),VM25PX), (TWV(234),HRTMAX), (TWV(242),URX),	003500S1
4	(TWV(245),UTX), (TWV(248),JNX), (TWV(252),VE28TP),	003600S1
5	(TWV(253),VE28RP), (TWV(254),DF29P), (TWV(256),QTHETM),	003700S1
6	(TWV(259),DAT20P), (TWV(260),TIM20P), (TWV(266),REVEOP)	003800S1
	EQUIVALENCE (ELTMNP(2),ELTMXP)	003900S1
	EQUIVALENCE (TWV(35),DATELP), (TWV(36),TIMELP),	004000S1
1	(TWV(57),RM8PX), (TWV(202),RE29P), (TWV(381),ALPHA),	004100S1
2	(VAR(97),DATE), (VAR(98),TIME), (FLT(24),RM9R)	004200S1
	EQUIVALENCE (TWV(383),REV2MN),	004300S1
1	(TWV(384),REV2MX), (TWV(385),IFLY), (TWV(386),TFLMIN),	004400S1
2	(TWV(387),TFLMAX), (TWV(394),TMMAX), (TWV(197),DAT29P),	004500S1
3	(TWV(198),TIM29P)	004600S1
	DIMENSION ELTMIN(2), SLT30P(2), CLT30P(2), ELTMNP(2),	004700S1
1	VM23PX(3), RM23PX(3), URX (3), JTX (3), UNX (3),	004800S1
2	HML0PX(3), RE28PX(3), VM8PX (3), VM21PX(3), RS23PX(3),	004900S1
3	RM25PX(3), VM25PX(3), TEMP1 (3), TEMP2 (3), TEMP3 (3),	005000S1
4	TEMP4 (3), TAJL (2), HML (3), RM20PX(3), VM20PX(3)	005100S1
5	TL (5), ALFA (2), TLP (5), DW (9), DV (9),	005200S1
6 W	(10)	005300S1
		005400S1

```

C
REVEOP=REVEO
RMSIP=RMSI
QDELT8=.1
QALF28=.01
QEL30=.1
TYPREN=1.
TPFREN=1.
RE11P=REGEO0+ALTATM
3TA11P=3TA11R
RLOP=RLO
RE29P=REGEO0+ALTATM
3TA29P=3TA29R
DO 10 I=1,2
TEMP50=DTOR*ELTMIN(I)
EL1MNP(I)=RTOD*ATAN((1.-FLAT)**2*SIN(TEMP50)/COS(TEMP50))
TEMP50=DTOR*ELTMNP(I)
SLT30P(I)=SIN(TEMP50)
10 CLT30P(I)=COS(TEMP50)
EL130P=(ELTMNP(I)+ELTMXP)/2.
ELN30P=-150.
ELT30R=ELT30P
ELN30R=ELN30P
RHETAM=33.3
IL00P=1
C
PERL0P=2.*PI*RLOP*SQRT(RLOP/GMM)
C
VCIR=SQRT(GMM/RLO)
DLV0IM=3400.
DLV20P=0.
DLV55P=0.
DLV26P=0.
CALL WG1BDJ
DV9MX=304.7*GSTD*LOG(W(4)/(W(4)-18550.))
IPRABT=0
TA9=7200.
DELPHI=2.
TOL=25.
SDV9AP=1000000.
C
WRITE(6,15)DW,DV
15 FORMAT('0INPUT DATA'// DW',9F1n.1// DV',9F10.1)
CALL PRINTR(0,'ELN30PTA9 DV9MX FUELMXW(1) ','
• ELN30P,TA9,DV9MX,FUELMX,W(1))
• CALL PRINTR(0,'HRSTAYREVEO REVLO1REVL02 ','
• HRSTAY,REVEO,REVLO1,REVLO2,A)
C
INJM=0
C
ALPHA=220.
IALPHA=1
ICOUNT=1
C
2000 CALL STERN
CALL ABORT(TA9,DV9AP,TIMAB,ABINC,ABPCH,IPRABT)
WRITE(6,7) ALPHA,DV9AP
00550051
00560051
00570051
00580051
00590051
00600051
00610051
00620051
00630051
00640051
00650051
00660051
00670051
00680051
00690051
00700051
00710051
00720051
00730051
00740051
00750051
00760051
00770051
00780051
00790051
00800051
00810051
00820051
00830051
00840051
00850051
00860051
00870051
00880051
00890051
00900051
00910051
00920051
00930051
00940051
00950051
00960051
00970051
00980051
00990051
01000051
01010051
01020051
01030051
01040051
01050051
01060051
01070051
01080051
01090051
01100051
01110051

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7 FORMAT(10X,'ALPHA=',F3.2,10X,'JV9=',F16.4) 01120051
IF(ICOUNT.EQ.1.AND.DV9AP.LT.DV9MX) GO TO 2400 01130051
IF(ABS(DV9AP-DV9MX).LT.TOL/2..OR.ICOUNT.EQ.10)GO TO 2400 01140051
IF(ICOUNT.EQ.1)GO TO 2100 01150051
IF(ICOUNT.GT.2.OR.(DV9MX-DV9AP)/(DV9MX-SDV9AP).LT.0.)GO TO 2300 01160051
C 01170051
2100 SALPHA=ALPHA 01180051
DV93K=SDV9AP 01190051
SDV9AP=DV9AP 01200051
ICOUNT=2 01210051
ALPHA=ALPHA+2.*IALPHA 01220051
IF((ALPHA.LT.320.1.AND.DV9AP.LT.DV9BK+100.).OR.IALPHA.LT.0)GO TO 01230051
2000 01240051
    WRITE(6,8) ERG7P 01250051
8 FORMAT('0      ***THIS ENERGY---', E20.8,' IS UNABORTABLE ***')01260051
    RETURN 01270051
C 01280051
2300 TEMP=(DV9MX-DV9AP)*(ALPHA-SALPHA)/(DV9AP-SDV9AP) 01290051
SALPHA=ALPHA 01300051
SDV9AP=DV9AP 01310051
ALPHA=ALPHA+TEMP 01320051
ICOUNT=ICOUNT+1 01330051
GO TO 2000 01340051
C 01350051
2400 IF(IALPHA.LT.0)GO TO 2410 01360051
ALFA(1)=ALPHA 01370051
ICOUNT=1 01380051
ALPHA=320. 01390051
IALPHA=-1 01400051
GO TO 2000 01410051
2410 ALFA(2)=ALPHA 01420051
ALPHA=ALFA(1)-2. 01430051
2420 IF(ABS(ALPHA-ALFA(2)).LT..01)RETURN 01440051
ALPHA=ALPHA+2. 01450051
IF(ALPHA.GT.ALFA(2))ALPHA=ALFA(2) 01460051
C 01470051
CALL STERN 01480051
C 01490051
CALL ABORT(TA9,DV9AP,TIMAB,ABINC,ABPCH,IPRABT) 01500051
WRITE(6,2500)DATEF,ERG7P,ALPHA,DV9AP 01510051
2500 FORMAT(///' DATEF',F11.1,5X,'ERG7P',F12.0,5X,'ALPHA',F6.0,5X,,DV901520051
    .AP',F7.0//          T14,'PHI',T21,'TAU',T27,'DLV20  DLV55  DLV2601530051
    .  WGT',T57,'FUEL',T65,'SLSLAT',T75,'SLSLOV') 01540051
C 01550051
CALL CONIC(RM8PX,VM8PX,1,1,RL0,RM20PX,VM20PX,TEMP50) 01560051
RL0=RLOP 01570051
CALL ADDT(DAT8P,TIM8P,0.,TEMP50,DAT20P,TIM20P) 01580051
VM20=VALUE(VM20PX) 01590051
CALL CROSS(VM20PX,RM20PX,TEMP2,1) 01600051
CALL CROSS(RM20PX,TEMP2,TEMP4,1) 01610051
TEMP76=2.*VCIR*DOT(TEMP4,VM20PX) 01620051
C 01630051
TAJ=(REVL01+.5)*360. 01640051
ICOUNT=1 01650051
ITEST=1 01660051
C 01670051
IF(INJM.EQ.1)GO TO 3000 01680051

```

```

TMAX=TMMAX*24.                                     01690051
IF(IFLY.EQ.2)REVL02=REV2MN                      01700051
TEMP51=(REVL01+.5+AINTRHSTAY*SECHR/PERLOP+.25)+REVL02+1.)*PERLOP01710051
CALL ADDT(DAT20P,TIM20P,-DATELP,-TIMELP,DDAY,TTIME) 01720051
T0=DDAY*24.+TTIME+TEMP51)/3600.                  01730051
TG0=TMAX-T0                                      01740051
WRITE(6,2600)TG0                                01750051
2600 FORMAT('+'',T100,'TG0='',F12.4)             01760051
IF(TG0.GE.112.)GO TO 2900                      01770051
IF(TG0.LT.45.)RETURN                           01780051
HRTMXP=TG0-2.                                    01790051
PHI=0.                                         01800051
GO TO 3015                                      01810051
2700 ALF28P=90.                                 01820051
ELN30P=-160.                                    01830051
CALL ADDT(DAT23P,TIM23P,0.,TSTAY+(REVL02+1.)*PERLOP,01840051
.)
TEMP51=DEGCIR*(REVL02-AINTRHSTAY)                01850051
CALL ROTATE (RM23PX,HML0PX,TEMP51,RM25PX)      01860051
CALL ROTATE (VM23PX,HML0PX,TEMP51,VM25PX)      01870051
CALL HOME                                       01880051
CALL ADDT(DAT30P,TIM30P,-DATELP,-TIMELP,DDAY,TTIME) 01890051
TL(1)=DDAY*24.+TTIME/3600.                      01900051
TL(2)=TL(1)+24.                                01910051
TL(3)=TL(1)-24.                                01920051
TL(4)=TL(1)-48.                                01930051
TMAX=AMAX1(TMAX,T0+112.)                        01940051
DO 2800 I=1,4                                  01950051
2800 IF(TL(I).LE.TMAX.AND.TL(I).GE.(T0+45.))GO TO 2900 01960051
RETURN                                         01970051
2900 INJM=1                                    01980051
C
3000 DLV20P=DVL0IM                            01990051
TEMP=(VCIR**2+VM20**2-DLV20P**2)/TEMP76        02000051
IF(ABS(TEMP).GT.1.)RETURN                      02010051
PHI=-ARCCOS(TEMP)*RTOD                         02020051
C
3015 CALL ROTATE(TEMP4,RM20PX,PHI,VM21PX)      02030051
DO 3025 I=1,3                                  02040051
3025 VM21PX(I)=VM21PX(I)*VCIR                 02050051
CALL CROSS(RM20PX,VM21PX,HML,1)                02060051
IF(INJM.EQ.0)GO TO 6200                         02070051
C
3050 CALL ADDT(DAT20P,TIM20P,0.,PERLOP*TAU/360.,DATE,TIME) 02080051
IF(IEST.LE.2)DLV55P=0.                          02090051
CALL TAULIM(RM20PX,VM21PX,HML,DLV55P,TAUL,IORBIT) 02100051
C
6000 TAU=TAUL(1)                                02110051
IF(IEST.EQ.4)TAU=TAUL(2)                        02120051
6200 CALL ROTATE(RM20PX,HML,TAU,RM23PX)        02130051
TEMP51=PERLOP*TAU/360.                          02140051
CALL ADDT(DAT20P,TIM20P,0.,TEMP51,DAT23P,TIM23P) 02150051
DATE=DAT23P                                     02160051
TIME=TIM23P                                     02170051
CALL QMFIXP(1,RM23PX,RS23PX)                   02180051
IF(IEST.EQ.5)GO TO 7400                         02190051
C

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C           SIMULATE LUNAR STAY TIME AND CSM PLANE CHANGE          02250051
C
C   TSTAY=AIINT(HRSTAY*SECHR/PERLOP+.25)*PERLOP               02270051
C   CALL ADDT(DAT23P,TIM23P,0.,TSTAY,DATE,TIME)                 02280051
C   CALL QMFIXP(0,RS23PX,TEMP1)                                02290051
C   CALL CROSS(HML,TEMP1,TEMP2,1)                               02300051
C   CALL CROSS(TEMP1,TEMP2,TEMP3,0)                             02310051
C   PCHCMP=ABS(RTOD*ATAN(DOT(TEMP1,HML)/DOT(TEMP3,HML)))    02320051
C   DLV55P=VCIR*SQRT(2.-2.*COS(PCHCMP*DTOR))                02330051
C   TEMP51=VALUE(TEMP1)                                         02340051
C   TEMP50=RLO/TEMP51                                           02350051
C   DO 302 I=1,3                                              02360051
C   HML0PX(I)=TEMP3(I)/TEMP51                                 02370051
C   RM23PX(I)=TEMP50*TEMP1(I)                                02380051
302  VM23PX(I)=VCIR*TEMP2(I)                                02390051
     IF(INUM.EQ.0)GO TO 2700                                  02400051
C
C   CALL SNDHOM                                                 02410051
C
C   CALL WGTBJD                                                 02420051
C
C   SLSLAT=RTOD*ARSIN(RS23PX(3)/VALUE(RS23PX))              02430051
C   SLSLON=RTOD*ATAN2(RS23PX(2),RS23PX(1))                  02440051
C   WRITE(6,6100)PHI,TAJ,DLV20P,DLV55P,DLV26P,WGT,FUEL,SLSLAT,SLSLON 02450051
5100  FORMAT(9X,F8.2,4F7.0,2F8.0,F9.2,F11.2)                02460051
C
C   IF(ITEST.GT.2)GO TO 5800                                  02470051
C
C   IF(ABS(FUEL-FUELMX).LT.TOL.OR.(ICOUNT.EQ.10)GO TO 4000    02480051
C   IF(ICOUNT.EQ.1)GO TO 3400                                02490051
C   IF(ICOUNT.GT.2.OR.(FUELMX-SFUEL)/(FUELMX-FUEL).LT.0.)GO TO 35n0 02500051
C   IF(FUEL.GT.SFUEL.AND.FUEL.GT.FUELMX)GO TO 3450            02510051
C
C   3400  SFUEL=FUEL                                         02520051
C   SPHI=PHI                                               02530051
C   PHI=PHI+DELPHI                                         02540051
C   ICOUNT=2                                              02550051
3420  IF(PHI.GT.0.AND.(PHI-DELPHI).LT.-.1)PHI=0.             02560051
3010  DLV20P=SQRT(VCIR**2+VM20**2-TEMP76*COS(PHI*DTOR))    02570051
     GO TO 3015                                              02580051
C
C   3450  IF(ITEST.EQ.1)GO TO 2420                            02590051
3500  TEMP=(FUELMX-FUEL)*(PHI-SPHI)/(FUEL-SFUEL)            02600051
     SFUEL=FUEL                                         02610051
     SPHI=PHI                                               02620051
     PHI=PHI+TEMP                                         02630051
     ICOUNT=ICOUNT+1                                       02640051
     GO TO 3010                                              02650051
C
C   4000  IF(ITEST.EQ.2)GO TO 4500                            02660051
     WRITE(6,9001)PHI                                         02670051
9001  FORMAT('+'',T85,'PHIMIN'',F12.4)                      02680051
     CALL SAVE(1)                                            02690051
     DLV55P=10.                                             02700051
     GO TO 5700                                              02710051
C
C   4500  IF(PHI-OLDPHI.LT.3.5)GO TO 5710                    02720051
     02730051
     02740051
     02750051
     02760051
     02770051
     02780051
     02790051
     02800051
     02810051
     02820051

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PHI=OLDPHI          028300S1
DLV55P=10.          028400S1
GO TO 5700          028500S1
5710 WRITE(6,9002)PHI 028600S1
9002 FORMAT('+',T85,'PHIMAX',F12.4) 028700S1
CALL SAVE(2)        028800S1
GO TO 2420          028900S1
C
5000 ITEST=2         029000S1
ICOUNT=1            029100S1
PHI=PHI-DELPHI/2.  029200S1
GO TO 3010          029300S1
C
5700 PHI=PHI+DELPHI 029400S1
IF(PHI.GT.0.AND.(PHI-DELPHI).LT.-.1)PHI=0. 029500S1
OLDPHI=PHI          029600S1
ITEST=3             029700S1
ICOUNT=1            029800S1
SENS26=0.            029900S1
030000S1
030100S1
GO TO 3010          030200S1
C
5800 IF(ABS(FUEL-FUELMX).LT.TOL.OR.ICOUNT.EQ.10)GO TO 6500 030300S1
IF(IORBIT.EQ.1.AND.ITEST.EQ.4.AND.ICOUNT.EQ.1.AND.FUEL.LT.FUELMX) 030400S1
GO TO 7000          030500S1
IF(DLV55P.EQ.SDLV55.AND.ICOUNT.NE.1)GO TO 6500          030600S1
IF(ICOUNT.NE.1)SENS26=(DLV26P-SSDV26)/(DLV55P-SDLV55) 030700S1
IF(SENS26.LT.-.9)SENS26=-.9          030800S1
SDLV55=DLV55P          030900S1
SSDV26=DLV26P          031000S1
SDW=DW(1)            031100S1
031200S1
DO 5850 I=2,6        031300S1
SDW=SDW+DW(I)        031400S1
A=LOG((-FUELMX+w(1)-SDW-DW(7)*(1.-EXP(-(DV(8)+DV(9))*D20))- 031500S1
DW(8)*(1.-EXP(-DV(9)*D20)))/W(7))          031600S1
DLV55P=DLV55P-(A/D20+DV(7)+DV(8)+DV(9))/(1.+SENS26) 031700S1
IF(DLV55P.LE.0.)GO TO 5000          031800S1
ICOUNT=ICOUNT+1        031900S1
GO TO 3050          032000S1
C
6500 IF(ITEST.EQ.4)GO TO 7000          032100S1
ITEST=4             032200S1
ICOUNT=1            032300S1
SENS26=0.            032400S1
TAJMIN=TAJ          032500S1
032600S1
WRITE(6,9003)TAJMIN 032700S1
9003 FORMAT('+',T85,'TAJMIN',F12.4) 032800S1
MMM=3               032900S1
IF(IORBIT.EQ.1)MMM=6 033000S1
CALL SAVE(MMM)        033100S1
IF(FUEL.GE.FUELMX+2.*TOL)GO TO 5700 033200S1
GO TO 6000          033300S1
C
7000 TAUMAX=TAJ        033400S1
IF(TAUMAX-TAUMIN.GT.180.1)TAUMAX=TAUMAX-180. 033500S1
WRITE(6,9004)TAJMAX 033600S1
9004 FORMAT('+',T85,'TAUMAX',F12.4) 033700S1
MMM=4               033800S1
033900S1

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IF(IORBIT.EQ.1)MMM=7          03400051
CALL SAVE(MMM)                03410051
MMM=5                         03420051
IF(IORBIT.EQ.1)MMM=8          03430051
ITEST=5                       03440051
DELT AJ=.25                   03450051
TAJ=TAJMIN                     03460051
GO TO 7500                     03470051
C
7400  SLSLATERTOD*ARSIN(RS23PX(3)/VALUE(RS23PX)) 03480051
SLSLOVERTOD*ATAN2(RS23PX(2),RS23PX(1))        03490051
CALL SAVE(MMM)                03500051
7500  TAJ=TAJ+DELT AJ         03510051
IF(TAJ.GE.TAJMAX)GO TO 5700   03520051
GO TO 6200                     03530051
03540051
C
C
C
C           GRAND HOME
C
C
C
SUBROUTINE GNDHOM             03550051
C
IF(IFLY.EQ.2)REVL02=REV2MN   03560051
LOOP=1                         03570051
3001  CALL ADDT(DAT23P,TIM23P,0.,TSTAY+(REVL02+1.)*PERLOP,DAT25P,TIM25P) 03580051
TEMP51=DEGCIR*(REVL02-AINT(REVL02)) 03590051
CALL ROTATE (RM23PX,HML0PX,TEMP51,RM25PX) 03600051
CALL ROTATE (VM23PX,HML0PX,TEMP51,VM25PX) 03610051
ILOOP=1                         03620051
03630051
C
C           TRANSEARTH TRAJECTORY
C
IF(IFLY.NE.0) GO TO 3999     03710051
CALL FLYHOM                     03720051
RETURN                         03730051
3999  T0=(DAT25P-DATELP)*24.+ (TIM25P-TIME LP)/3600. 03740051
TGO=(TMAX+0.1)*24.-T0          03750051
TLMIN=T0+TFLMIN                03760051
TLMAX=T0+TFLMAX                03770051
03780051
IF(TGO.GE.TFLMAX) GO TO 4000  03790051
IF(TGO.LT.TFLMIN.AND.LOOP.EQ.1)GO TO 4999  03800051
IF(TGO.LT.TFLMIN.AND.LOOP.GT.1) GO TO 4950  03810051
03820051
HRTMXP=TGO-2.                  03830051
GO TO 4010                     03840051
03850051
4000  HRTMXP=TFLMAX-2.         03860051
4010  CALL FLYHOM               03870051
SOLV26=DLV26P                  03880051
SHRT=HRTMXP                     03890051
TLAND=(DAT29P-DATELP)*24.+ (TIM29P-TIME LP)/3600. 03900051
TL(1)=TLAND+24.                03910051
TL(2)=TLAND                     03920051
TL(3)=TLAND-24.                03930051
TL(4)=TLAND-48.                03940051
TL(5)=TLAND-72.                03950051
DO 4020 I=1,5                  03960051

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4020 TLP(I)=0. 03970051
ITLOOP=0 03980051
DO 4030 I=1,5 03990051
IF(TL(I).LT.TLMIN.OR.TL(I).GT.TLMAX.OR.TL(I).GT.TMMAX*24.) 04000051
GO TO 4030 04010051
ITLOOP=ITLOOP+1 04020051
TLP(ITLOOP)=TL(I) 04030051
4030 CONTINUE 04040051
IF(ITLOOP.NE.0) GO TO 4031 04050051
IF(LOOP.GT.1) GO TO 4950 04060051
GO TO 4999 04070051
4031 TLPMAX=TLP(1) 04080051
IF(TLPMAX.EQ.TLAND) GO TO 4100 04090051
HRTMXP=TLPMAX-T0+12. 04100051
CALL FLYHOM 04110051
IF(DLV26P.GT.SDLV26)GO TO 4100 04120051
SDLV26=DLV26P 04130051
SHRT=HRTMXP 04140051
4100 IF(PD26DT.LE.0.) GO TO 4901 04150051
4200 ILOOP=ILOOP+1 04160051
IF(ILoop.GT.ITLoop) GO TO 4901 04170051
HRTMXP=TLP(ILoop)-T0+12. 04180051
CALL FLYHOM 04190051
IF(DLV26P.GT.SDLV26) GO TO 4901 04200051
SDLV26=DLV26P 04210051
SHRT=HRTMXP 04220051
IF(PD26DT.LE.0.)GO TO 4901 04230051
GO TO 4200 04240051
4901 IF(LOOP.GT.1.AND.SDV26.LT.SDLV26) GO TO 4902 04250051
SDV26=SDLV26 04260051
SHRMX=SHRT 04270051
SREV2=REVL02 04280051
IF(IFLY.EQ.1) GO TO 4950 04290051
4902 REVL02=REVL02+3. 04300051
IF(REVL02.GT.REV2MX) GO TO 4950 04310051
LOOP=LOOP+1 04320051
GO TO 3001 04330051
4950 HRTMXP=SHRMX 04340051
REVL02=SREV2 04350051
DLV26P=SDV26 04360051
HRTEMX=HRTMXP 04370051
RETURN 04380051
4999 WRITE (6,4998) 04390051
4998 FORMAT(/'NO SOLUTION WITHIN FLIGHT TIME CONSTRAINT') 04400051
RETURN 04410051
C 04420051
C 04430051
C 04440051
C 04450051
C 04460051
C 04470051
C 04480051
SUBROUTINE FLYHOM 04490051
C 04500051
IELON=0 04510051
ELN30P=ELNMIN 04520051
3900 K21=1 04530051

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4000 CALL HOME          04540051
ELT30S=ELT30P          04550051
SELN30=ELN30P          04560051
STHM=THETAM            04570051
C                           04580051
C                           04590051
C   CALCULATE LIMITS ON ALF28P DUE TO MAXIMUM INCLINATION 04600051
C                           04610051
CSLT28=SQRT(RE28PX(1)**2+RE28PX(2)**2)/RE28P           04620051
SNLT28=RE28PX(3)/RE28P          04630051
ELT28P=RTOD*ATAN(SNLT28/CSLT28) 04640051
TEMP50=COS(DTOR*RIMAX)/CSLT28 04650051
IF(TEMP50.LT.1.) GO TO 4001    04660051
WRITE(6,9005)              04670051
9005 FORMAT(1H0,5X,'26HRIMAX CAN NOT BE SATISFIED') 04680051
CALL CHXKIT              04690051
4001 ALFMN1=90.*(TYPREV-1.)+RTOD*ATAN(TEMP50/SQRT(1.-TEMP50**2)) 04700051
ALFMX1=TYPREV*180.-ALFMN1      04710051
C                           04720051
C   CALCULATE LIMITS ON ALF28P DUE TO LATITUDE CONSTRAINT 04730051
C                           04740051
ALF1=0.                  04750051
ALF2=180.                04760051
PH0=ELTMAX               04770051
I=1                      04780051
4100 CSAL28=(SIN(PH0*DTOR)-SIN(ELT28*DTOR)*COS(DF30P*DTOR))/(COS(ELT28*DTOR)) 04790051
1P*DTOR)*SIN(DF30P*DTOR)) 04800051
IF(ABS(CSAL28).GT.1.) GO TO 4101    04810051
SNAL28=SQRT(1.-CSAL28**2)        04820051
ALF28=RTOD*ATAN2(SNAL28,CSAL28) 04830051
IF(ALF28.LT.90.) ALF1=ALF28    04840051
IF(ALF28.GT.90.) ALF2=ALF28    04850051
4101 I=I+1                  04860051
IF(I.GT.2) GO TO 4102          04870051
PH0=ELTMIN(1)                 04880051
GO TO 4100                  04890051
4102 ALFMN2=ALF1              04900051
ALFMX2=ALF2                  04910051
C                           04920051
C   CALCULATE LIMITS ON ALF28P 04930051
C                           04940051
AL28MN=AMAX1(ALFMN1,ALFMN2)+.01 04950051
AL28MX=AMIN1(ALFMX1,ALFMX2)-.01 04960051
IF(AL28MN.LE.AL28MX) GO TO 4199 04970051
WRITE(6,7001)                04980051
7001 FORMAT(1H0,5X,'EARTH LANDING AREA IS OUT OF RANGE') 04990051
CALL CHXKIT                 05000051
C                           05010051
C   CALCULATE OPTIMUM ALF28P 05020051
C                           05030051
4199 CALL CROSS(JRX,UTX,UNX,0) 05040051
DATE=DAT28P                 05050051
TIME=TIM28P                 05060051
CALL OPTALF(ALF28P,AL28MN,AL28MX,VE28TP,VE28RP,HMLOPX,ALF28T) 05070051
C                           05080051
5000 IF(<21.EQ.8)RETURN      05090051
IF(ABS(ALF28T-ALF28P).LT.QALF28) GO TO 5510 05100051

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D-14

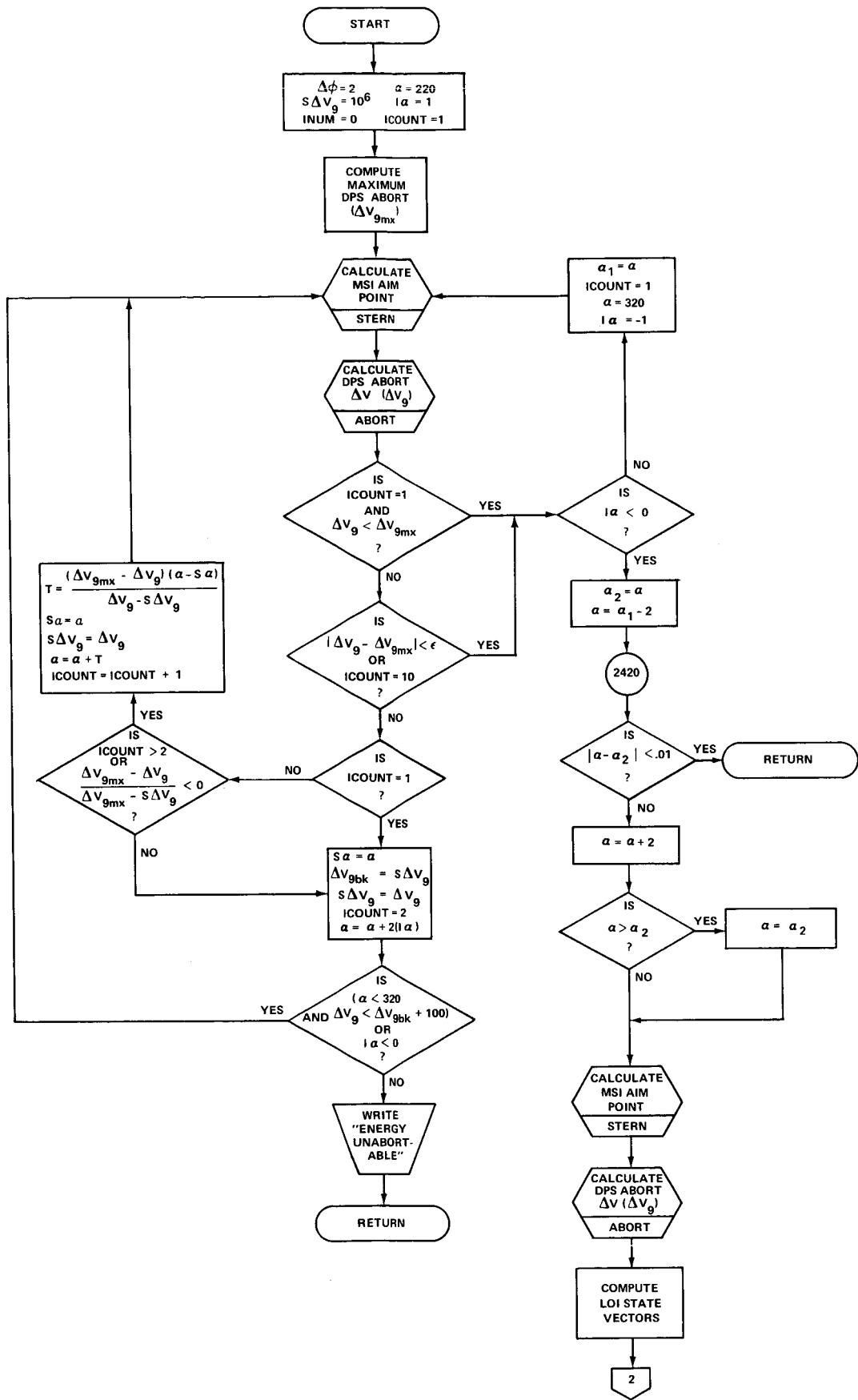


FIGURE D-1: ANLISIS FLOWCHART

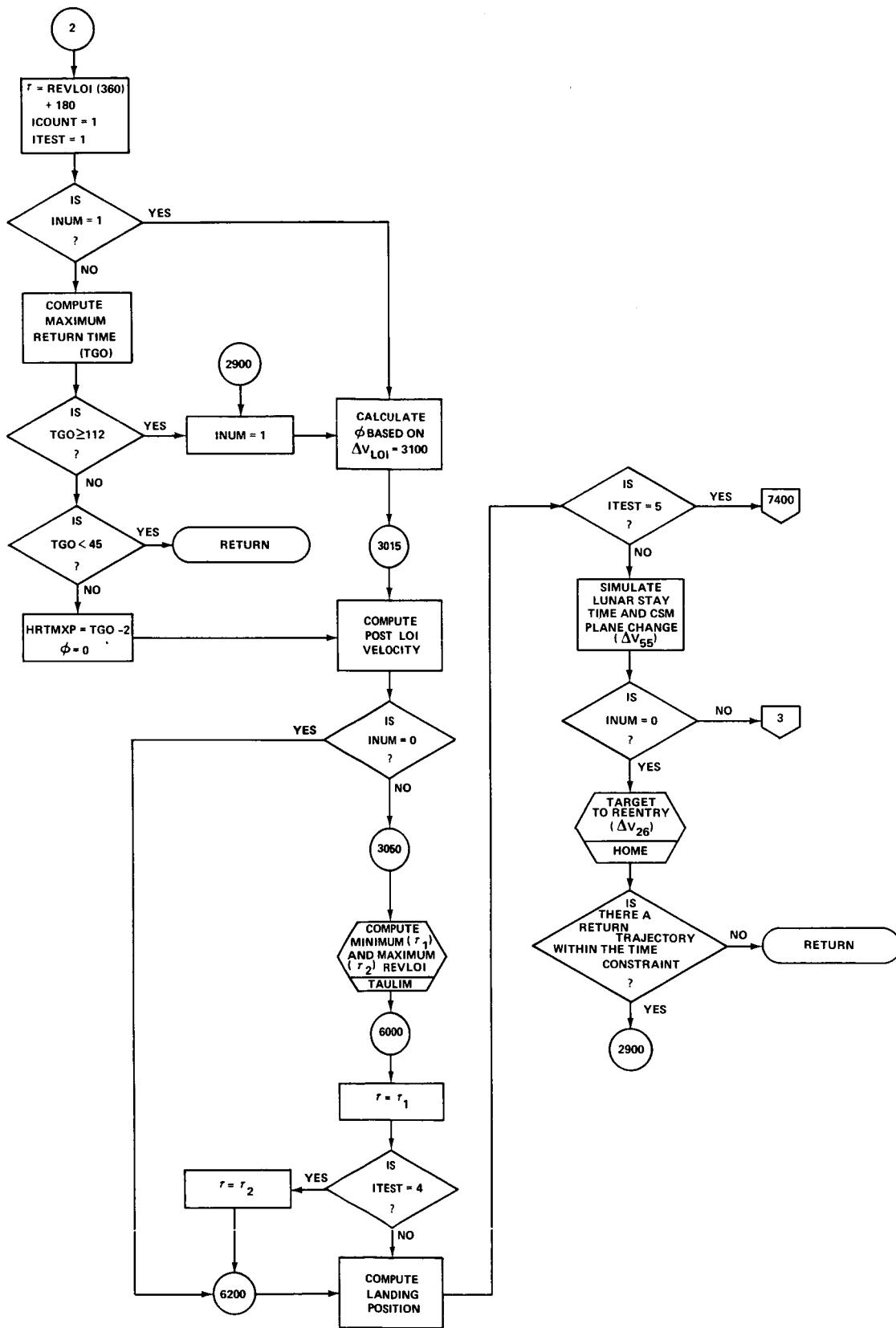


FIGURE D-2: ANLSIS FLOWCHART (CONT.)

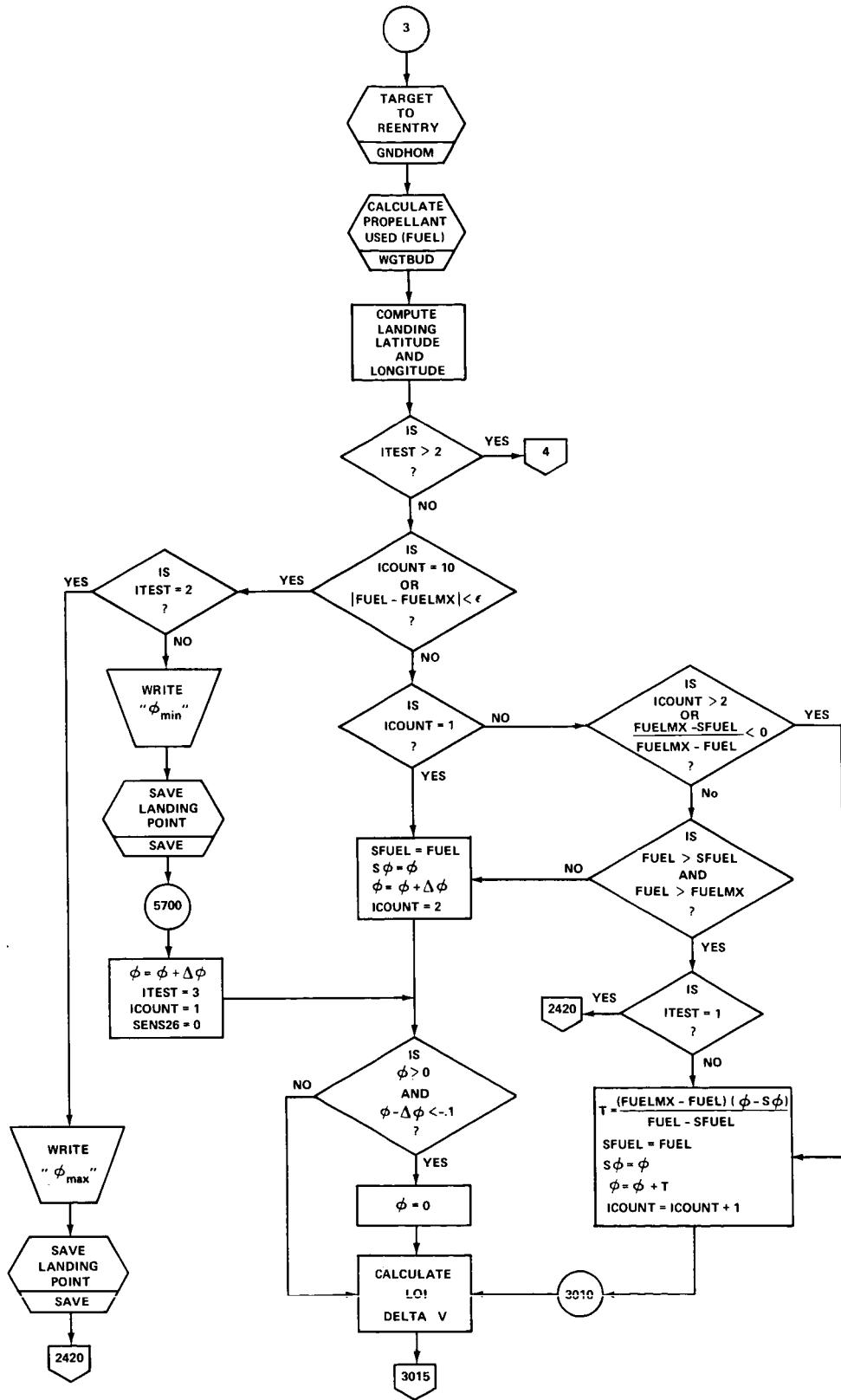


FIGURE D-3: ANLISIS FLOWCHART (CONT.)

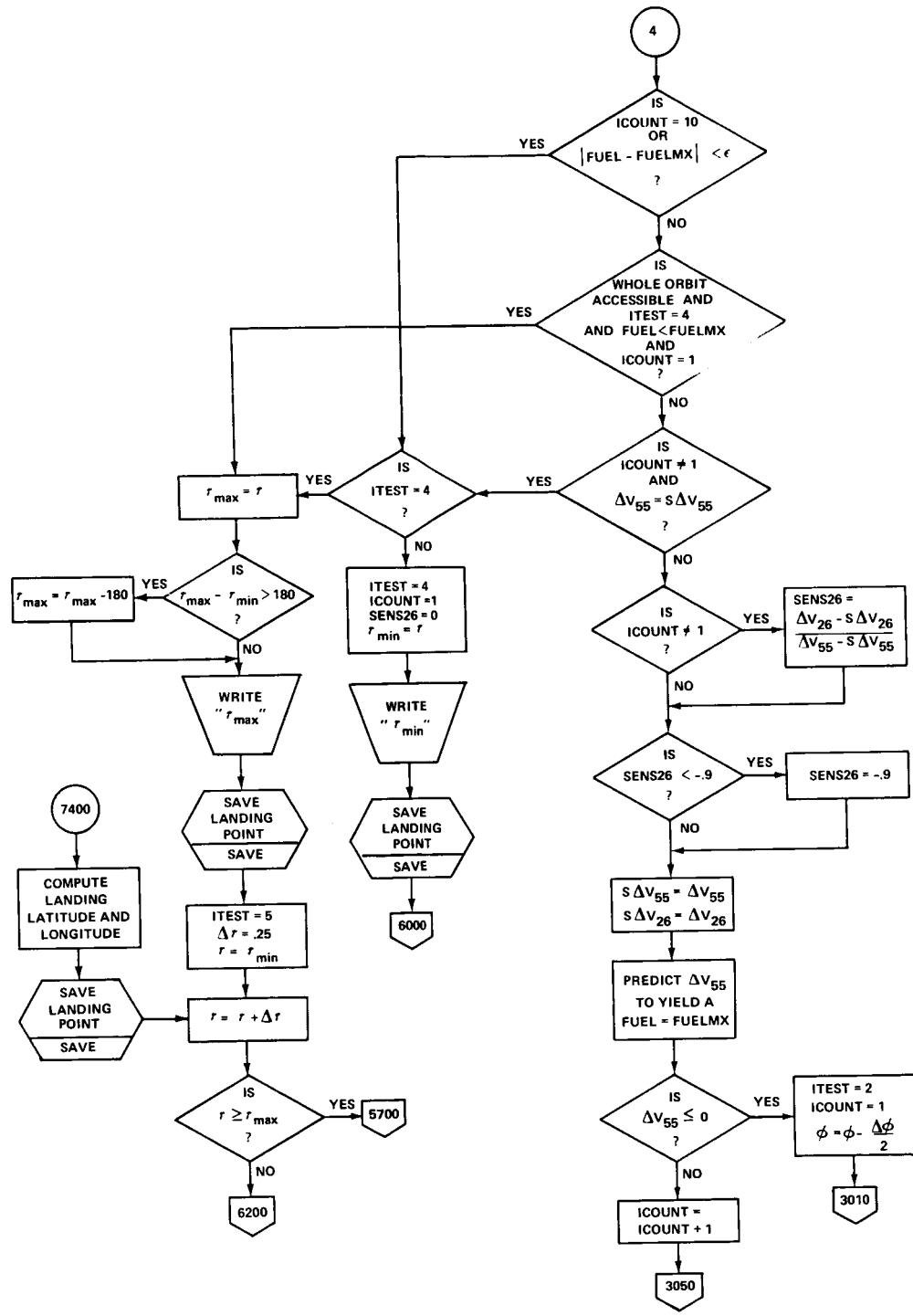


FIGURE D-4: ANLIS FLOWCHART (CONT.)

APPENDIX E

PLOT

Calling Sequence: CALL PLOT

Purpose: To produce a printer plot of the entire periphery matrix, to smooth the periphery matrix and then plot the smoothed version on the SC4020 plotter, and to compute the mean arrival time using the data matrix.

Input:*

SLON(241) - Longitude of landing
SLAT(241,2) - Minimum and maximum latitude of landing
ITVAL(6,241) - Data matrix corresponding to boundary matrix

*For further detail see outputs of subroutine ANLSIS in Appendix D.

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C          000100A1
C          SUBROUTINE PLOT                         000200A1
C          COMMON/VALUES/SLON(241),SLAT(241,2),ITVAL(6,241) 000300A1
C          REAL INCHES                           000400A1
C          WRITE(6,2)                            000500A1
C          FORMAT('1')                           000600A1
2          DO 35 L=6,7                          000700A1
35         WRITE(L,1)(SLON(I),(SLAT(I,<),<=1,2),(ITVAL(J,I),J=1,6),I=1,241) 001000A1
1          FORMAT(F6.1,2F7.2,6I10)                001100A1
C          D=0.                                001200A1
DATE=0.                           001300A1
DO 40 I=1,241                     001400A1
DO 40 J=3,6,3                     001500A1
IBLK=MOD(ITVAL(J,I),100000)      001600A1
IF(IBLK.NE.0)D=D+1.               001700A1
40        DATE=IBLK+DATE                 001800A1
IF(D.GT.0)DATE=DATE/100.          001900A1
TIME=AMOD(DATE,100.)*864.        002000A1
DATE=INT(DATE/100.)+2441000.5   002100A1
HRS=TIME/3600.                   002200A1
DEG=HRS*12.19/24.                002300A1
SCALE=.2                          002400A1
INCHES=DEG*SCALE                 002500A1
CALL DANDT(DATE,TIME,IMON,IDAY,IYR,IHR,IMIN,SEC) 002600A1
WRITE(6,3)DATE,TIME,IMON,IDAY,IYR,HRS,DEG,INCHES 002700A1
WRITE(7,4)DATE,TIME,IMON,IDAY,IYR,HRS,DEG,INCHES 002800A1
5          FORMAT('UMEAN ARRIVAL TIME',F11.1,F9.1,3X,A3,I3,I5,F7.2,5X,'DFG',002900A1
     * F8.3,5X,'INCHES',F7.3)                  003000A1
4          FORMAT(F11.1,F9.1,3X,A3,I3,I5,3F8.3) 003100A1
C          003200A1
          003300A1
DO 10 I=1,241                     003400A1
DO 10 J=1,2                         003500A1
10        CALL COLECT('SLSLAT',SLAT(I,J))      003600A1
CALL COLECT('SLSLON',SLON(I))       003700A1
CALL TITLE                           003800A1
CALL PLCHAR(0)                      003900A1
CALL PLTICS('SLSLAT',-75.,75.)     004000A1
CALL PLTICS('SLSLON',-90.,90.)     004100A1
CALL PTX('SLSLON','SLSLAT')        004200A1
CALL CULOUT('SLSLAT')              004300A1
CALL CULOUT('SLSLON')              004400A1
C          004500A1
CALL PLCHAR(0)                      004600A1
IPLOT=0                            004700A1
IPLOT=0                            004800A1
DO 65 JJ=1,2                        004900A1
IF(JJ.EQ.2)GO TO 12                005000A1
ISTART=1                           005100A1
IEND=121                           005200A1
GO TO 15                           005300A1
12        ISTART=121                  005400A1

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IEND=241          005500A1
15    CALL PLTSIM(1)          005600A1
C
DO 60 J=1,2          005700A1
DO 50 I=ISTART,IEND          005800A1
C
IF(ABS(SLAT(I,J)).GT.90.5)GO TO 20          005900A1
C
IF(I.EQ.IEND.OR.IPLOT.EQ.0)GO TO 19          006000A1
IF(ABS(SLAT(I+1,J)).GT.90.5)GO TO 19          006100A1
M1=IBASE+1          006200A1
M2=I+1          006300A1
DO 17 M=M1,M2          006400A1
SM=((SLON(M)-SLON(IBASE))*(SLAT(M2,J)-SLAT(IBASE,J))-(SLAT(M,J)-
      SLAT(IBASE,J))*(SLON(M2)-SLON(IBASE)))/SQRT((SLON(IBASE)-SLON(M2))**2+
      (SLAT(IBASE,J)-SLAT(M2,J))**2)          006500A1
17    IF(J.EQ.1)SM=-SM          006600A1
IF(SM.LT.-.2.0R.SM.GT.2.)GO TO 19          006700A1
GO TO 50          006800A1
19    IBASE=I          006900A1
C
CALL COLECT('SLSLAT',SLAT(I,J))          007000A1
CALL COLECT('SLSLON',SLON(I))          007100A1
IPLOT=IPLOT+1          007200A1
GO TO 50          007300A1
C
17    IBASE=I          007400A1
C
CALL COLECT('SLSLAT',SLAT(I,J))          007500A1
CALL COLECT('SLSLON',SLON(I))          007600A1
IPLOT=IPLOT+1          007700A1
GO TO 50          007800A1
C
20    IF(IPLOT.GT.0)CALL PLOT2          007900A1
CONTINUE          008000A1
50    IF(IPLOT.GT.0)CALL PLOT2          008100A1
60    IF(IPLOT.EQ.0)CALL PLOTBL          008200A1
65    RETURN          008300A1
C
SUBROUTINE PLOT2          008400A1
IF(IPLOT.EQ.1)GO TO 100          008500A1
CALL PLTICS('SLSLAT',-40.,50.)          008600A1
CALL PLTICS('SLSLON',-90.,0.)          008700A1
IF(JJ.EQ.2)CALL PLTICS('SLSLON',0.,90.)
CALL PLTDEN('SLSLAT',-90.)
CALL PLTDEN('SLSLON',-90.)
CALL QTX('SLSLON','SLSLAT')
IPLOT=1
100   CALL CJLOUT('SLSLAT')
CALL CJLOUT('SLSLON')
IPLOT=0
RETURN
C
SUBROUTINE PLOTBL          009100A1
CALL COLECT('SLSLAT',0.)
CALL COLECT('SLSLON',-90.)
CALL COLECT('SLSLAT',0.)
CALL COLECT('SLSLON',-90.)
IPLOT=2
CALL PLOT2
RETURN
C

```

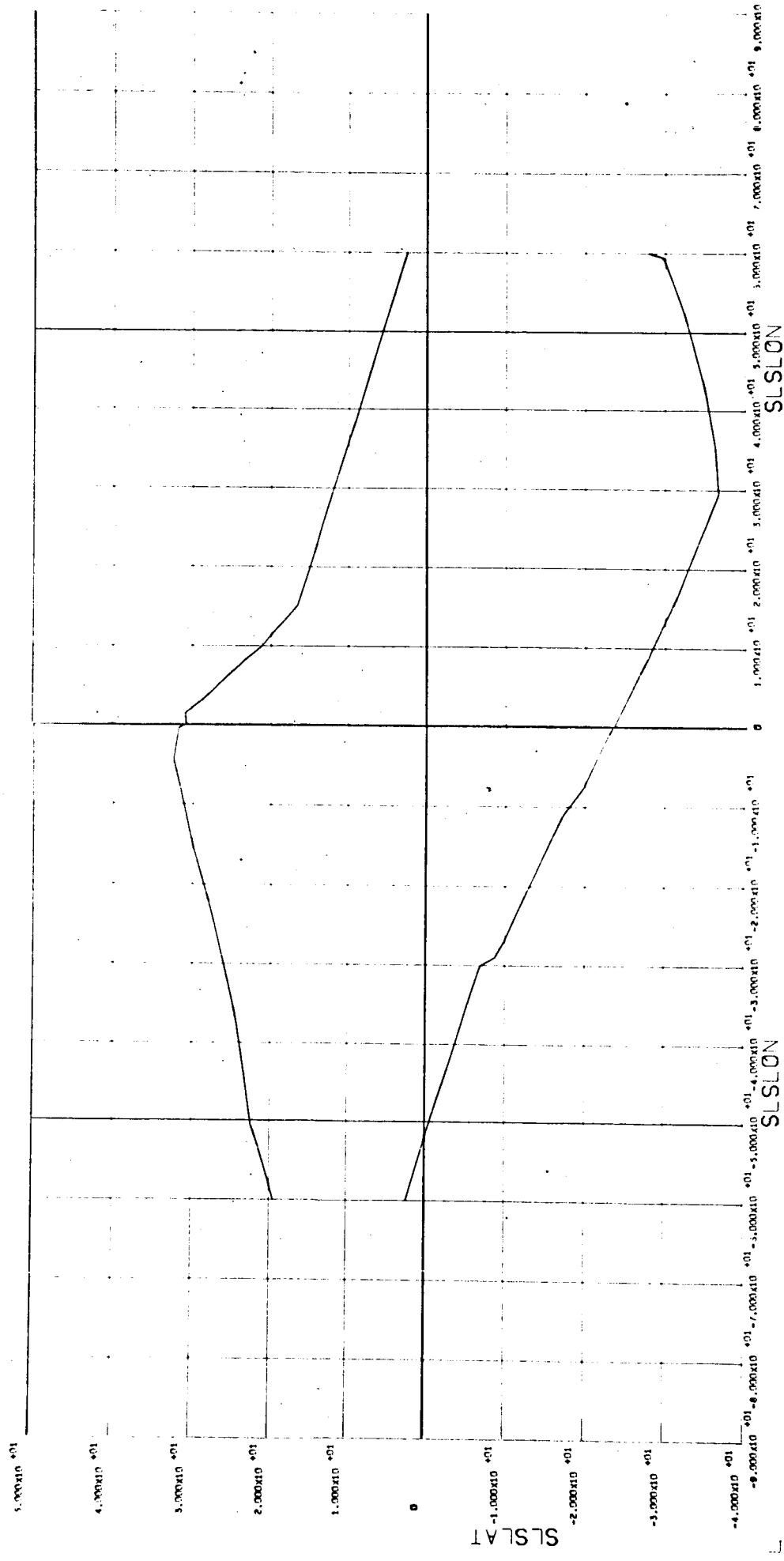



FIGURE 1: SAMPLE SC 4020 PLOT

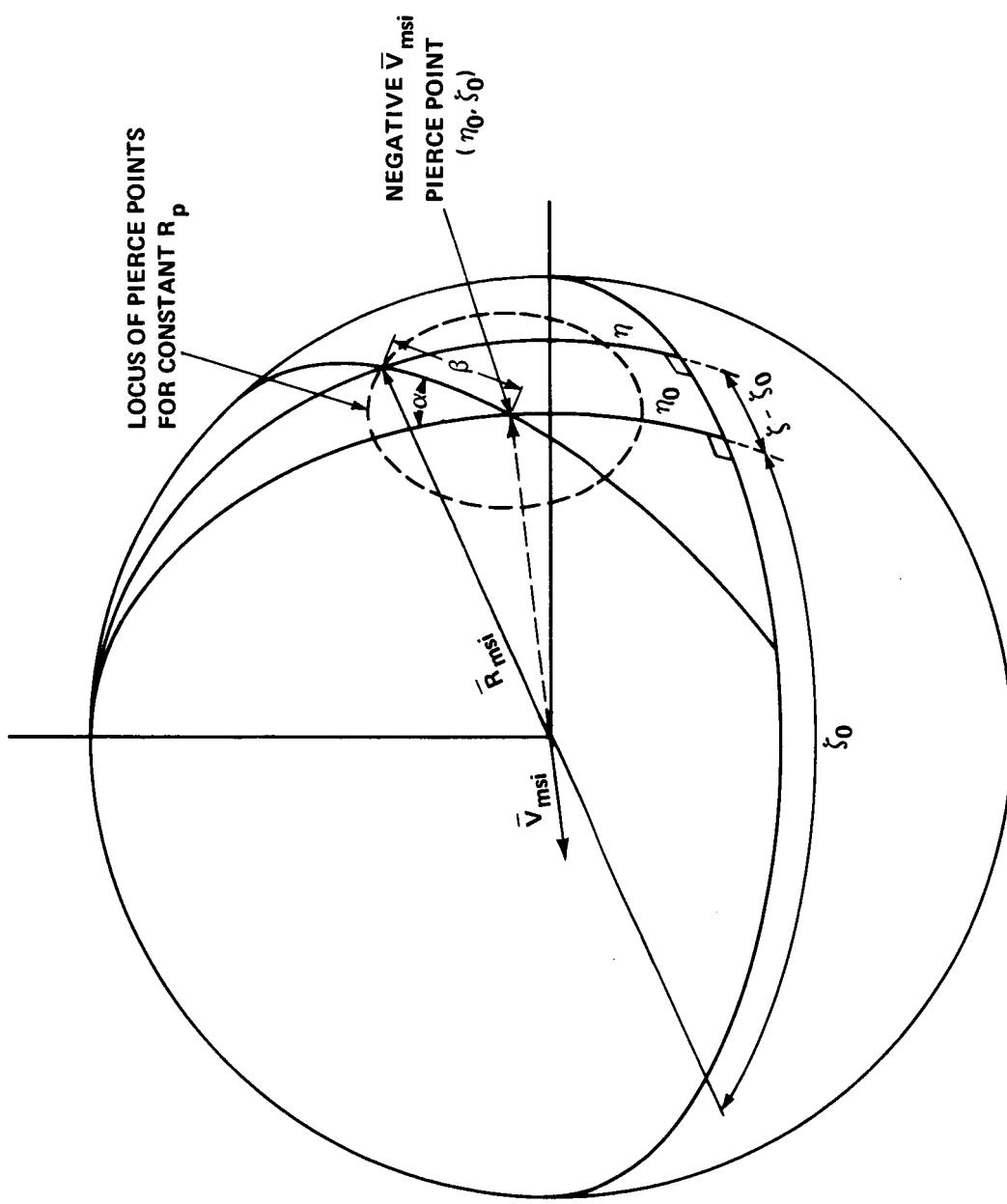


FIGURE 2: MSI ENTRANCE GEOMETRY

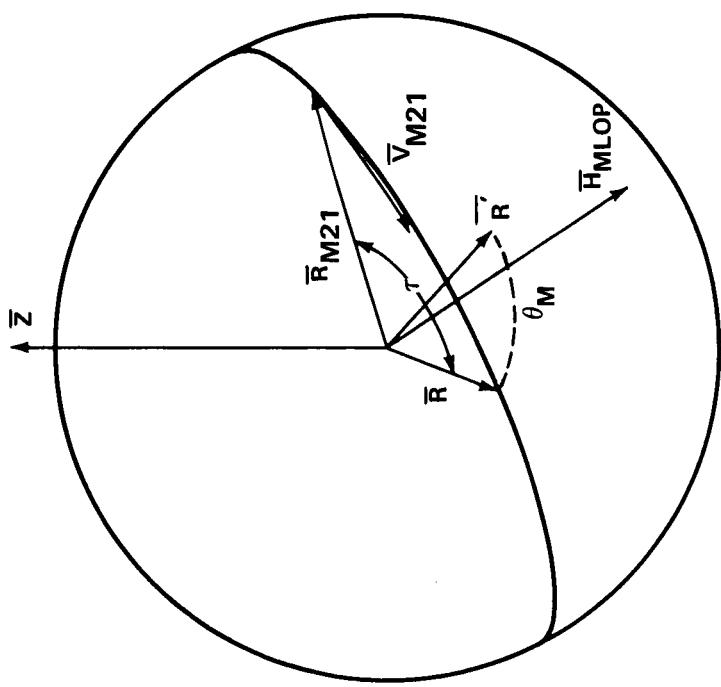


FIGURE 3: LUNAR ORBIT GEOMETRY

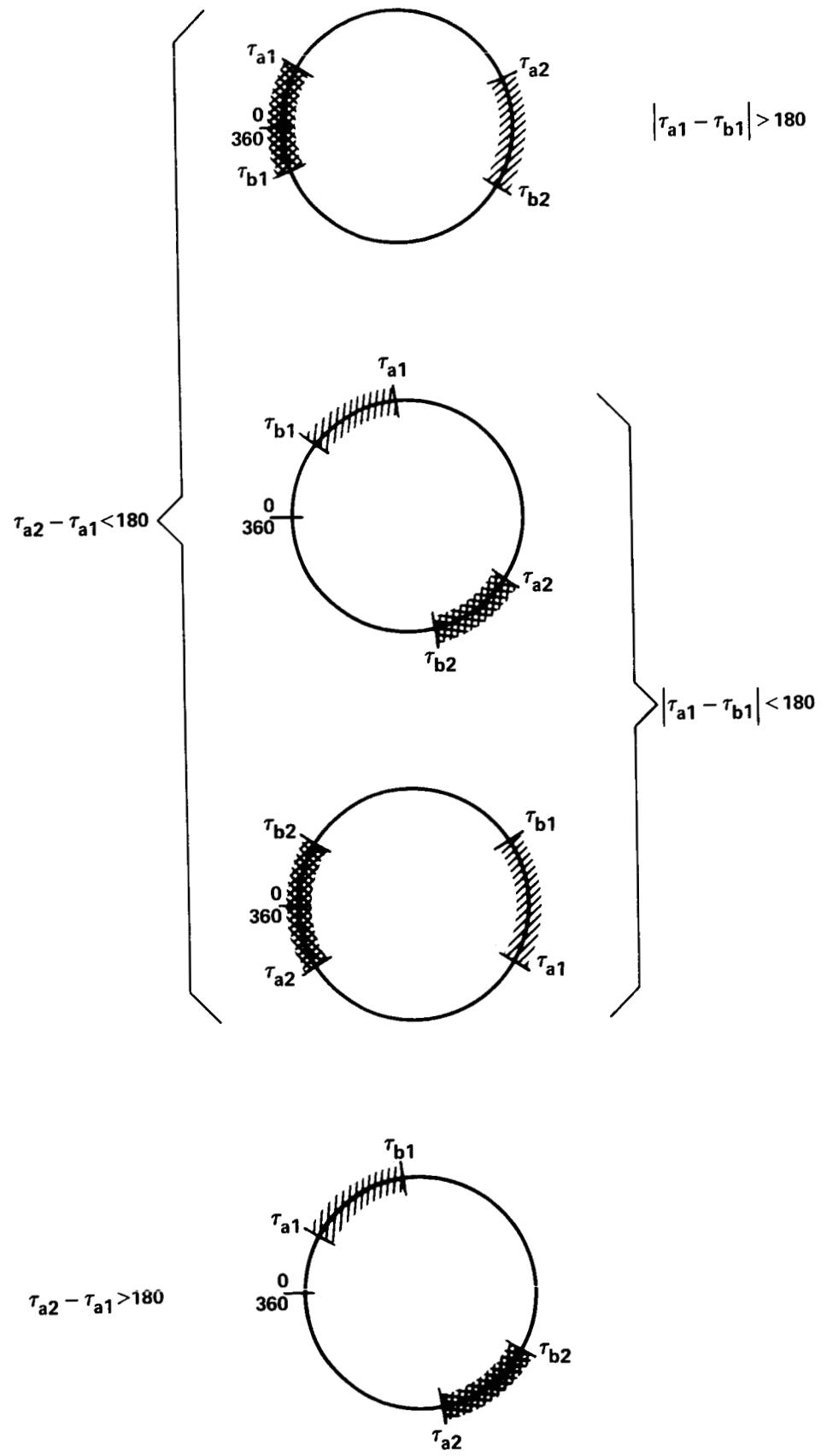


FIGURE 4: POSSIBLE τ LIMITS

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